# SEISMIC ANALYSIS OF AN ELEVATED WATER TANK CONSIDERING THE SLOSHING EFFECT 

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#### Abstract

The main objective of the present study is to evaluate the performance and behaviour of intze type of elevated water tank having radial staging configuration undertaking the parameter like base shear, base moment, top displacement, time period during empty and full tank condition considering the fixity condition. Further the effect of subsoil conditions on the seismic response of the tank has been studied by considering soil structure interaction (SSI). Also, the sloshing effect of liquid in the tank during dynamic loading has been considered.

The study consists of the analysis and design of the Intze type elevated water tank of capacity 1MLD which is resting 16 m above ground level on the staging containing 8 columns. The depth of the foundation is 1.2 m below ground level. The location of the tank considered in seismic zone II. Numerical analysis has been carried out using FEM based software SAP 2000. It is observed from the study that the base shear and base moment in full tank condition tank is slightly higher than empty tank due to absence of water load. By providing the free board height of 1.8 m which is greater than the sloshing wave height of 0.386 m we can reduce the additional stresses coming on the top dome. Since total base shear and base moment in tank full condition are more than that total base shear and base moment in tank empty condition, design will be governed by tank full condition.


Key Words: Sloshing effect, Intze tank, Impulsive pressure, Convective pressure, soil structure interaction.

## 1. INTRODUCTION

Water is life line for every kind of creature in this world. All around the world liquid storage tanks are used extensively by municipalities and industries for water supply, firefighting systems, inflammable liquids and other chemicals. Thus, Water tanks plays a vital role for public utility as well as industrial structure having basic purpose to secure constant water supply from longer distance with sufficient static head to the desired location under the effect of gravitational force. Storage reservoirs and overhead tank are used to store water, liquid petroleum, petroleum products and similar liquids. All tanks are designed as crack free structures to eliminate any leakage. Water or raw
petroleum retaining slab and walls can be of reinforced concrete with adequate cover to the reinforcement.

In general, there are three kinds of water tanks i.e. tank resting on ground, underground tanks and elevated tanks. Elevated tanks are supported on staging which may consist of masonry walls, R.C.C. tower or R.C.C. columns braced together. The walls are subjected to water pressure. The base has to carry the load of water and tank load. The staging has to carry load of water and tank. The staging is also designed for wind forces. From design point of view the tanks may be classified as per their shape- Rectangular tanks, Circular tanks, Intze type tanks. Spherical tanks conical bottom tanks and suspended bottom tanks. In water retaining structures a dense impermeable concrete is required therefore, proportion of fine and coarse aggregates to cement should be such as to give high quality concrete.

### 1.1 SEISMIC ANALYSIS OF ELEVATED WATER TANK

Equivalent static analysis of elevated water tanks is the conventional analysis based on the conversion of seismic load in equivalent static load. IS: 1893-2016 has provided the method of analysis of elevated water tank for seismic loading. Historically, seismic loads were taken as equivalent static accelerations which were modified by various factors, depending on the location's seismicity, its soil properties, the natural frequency of the structure, and its intended use. Elevated water tank can be analysed for both the condition i.e. tank full condition and tank empty condition. For both the condition, the tank can be idealized by one mass structure. For equivalent static analysis, water-structure interaction shows, both water and structure achieve a pick at the same time due to the assumption that water is stuck to the container and acts as a structure itself and both water and structure has same stiffness.

Most elevated tanks are never completely filled with liquid. Hence a two-mass idealization of the tank is more appropriate as compared to a one mass idealization, which was used in IS 1893: 1984. Two mass model for elevated tank was proposed by Housner (1963) and is being commonly used in most of the international codes. Here the entire structure and liquid which is in direct contact with the structure is considered as one mass called impulsive mass and the remaining liquid portion is considered as other mass called convective mass.

Gaikwad Madhukar and Mangulkar Madhuri (2013), Ankita Patel and BalChandra (2014), Neha Walde, Sakshi Manchalwar et al (2015), Abhijeet Babar and Jadhav (2016), Prashant Bansode et al. (2017), Ajmal Tokhi and Sahil Arora (2019) and many more have carried out studies on elevated water tank considering differentstaging conditions, different zonal conditions, different tank shapes and capacities. However, the effect of sloshing of water due to hydrodynamic nature deserves the performance of water tanks.

## 2. SCOPE AND OBJECTIVES

1. The proposed work involves the study on seismic behaviour of elevated water tank considering sloshing effects due to water.
2. Further analysis will be carried out for tank empty and full condition.

The objectives of the proposed study are

1. To evaluate the dynamic displacement of water tank subjected to ground motion using response spectrum analysis.
2. To evaluate the associated base shear due to dynamic loading.
3. Analyse the tank considering the soil structure interaction effects

## 3. MODELLING AND ANALYSIS

The study consists of the analysis and design of the Intze type of elevated water tank of capacity 1MLD which is resting 16 m above ground level on the staging with 8 columns. The depth of the foundation is 1.2 m below ground level. M30 grade concrete and Fe 415 grade steel are considered as material properties. The location of the tank is considered in seismic zone II.


Fig -1: Intze tank

Table -1: Details of sizes of various components obtained from design.

| Component s | Sizes(mm) | Calculations | Weight (KN) |
| :---: | :---: | :---: | :---: |
| Top dome | 100 thick | $2 \pi \times 9.35 \times 1.8 \times 0.1 \times 25$ | 264.36 |
| Top ring beam | $500 \times 410$ | $\pi \times 16.4 \times 0.5 \times 0.41 \times 25$ | 264.05 |
| Wall | 300 thick | $\pi \times 16 \times 0.3 \times 4 \times 25$ | 1507.97 |
| Bottom ring beam 1 | $1000 \times 600$ | $\pi \times 16.4 \times 0.6 \times 1 \times 25$ | 772.83 |
| Conical dome | 500 thick | $\begin{aligned} & \pi \times(6.9+5.3) \times \\ & \sqrt{(6.9-5.3)^{2}+3^{2}} \times 0.5 \times 2 \end{aligned}$ | 1628.91 |
| Bottom dome | 280 thick | $2 \pi \times 4.305 \times 1.6 \times 0.28 \times 25$ | 108.19 |
| Bottom circular beam | $700 \times 1200$ | $\pi \times 10.6 \times 0.7 \times 1.2 \times 25$ | 699.31 |
| Columns | 700 dia | $\frac{\text { 프́ }}{4} \times(0.7)^{2} \times 16 \times 8 \times 25$ | 1231.50 |
| Braces | $300 \times 700$ | $0.3 \times 0.7 \times 4.05 \times 24 \times 25$ | 510.3 |
| Water |  | $\begin{aligned} & \frac{\text { 프 }}{4} \times 16^{2} \times 4 \times 9.81+\left(V_{\text {cone }}\right. \\ & \left.V_{\text {Bdome }}\right) \times 9.81 \end{aligned}$ | 11053.63 |

Table -2: Parameters after numerical analysis for full tank condition

| MODES | IMPULSIVE | CONVECTIVE |
| :--- | :--- | :--- |
| TIME PERIOD | 1.19 sec | 4.15 sec |
| DESIGN HORIZONTAL <br> SEISMIC COEFFICIENT | 0.028 | 0.014 |
| BASE SHEAR | 339.81 KN | 70.987 KN |
| BASE MOMENT | 7192.903 KNm | 1533.310 KNm |

Table -3: Parameters after numerical analysis for empty tank condition

| TIME PERIOD |  |
| :--- | :--- |
| DESIGN HORIZONTAL SEISMIC <br> COEFFICIENT | 0.883 sec |
| BASE SHEAR | 0.0395 |
| BASE MOMENT | 4683.592 KN |

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Table -4: hydrodynamic pressure calculations for full tank condition

| Hydrodynamic <br> pressure <br> calculations | 1. Impulsive pressure on wall $=1.45 \mathrm{KN} / \mathrm{m}^{2}$ <br> 2.Impulsive pressure on slab base $=1.082 \mathrm{KN} / \mathrm{m}^{2}$ <br> 3. Convective pressure on wall $=0.709 \mathrm{KN} / \mathrm{m}^{2}$ <br> 4.Convective pressure on slab base $=0.219 \mathrm{KN} / \mathrm{m}^{2}$ |
| :--- | :--- |
| Pressure due to <br> inertia of wall. | $0.195 \mathrm{KN} / \mathrm{m}^{2}$ |
| Pressure due to <br> vertical excitation. | $2.14 \mathrm{KN} / \mathrm{m}^{2}$ |
| Maximum <br> hydrodynamic <br> pressure. | $2.708 \mathrm{KN} / \mathrm{m}^{2}$ |
| Hydrostatic <br> pressure. <br> $\rho \times \mathrm{g} \times \mathrm{h}$ | $68 \mathrm{KN} / \mathrm{m}^{2}$ |

## 4. Analysis results of the elevated water tank

### 4.1 Empty tank condition for fixed base model.

Here the analysis is carried out by considering only the dead load and its combination. All the column supports are fixed. Response spectrum and time history analysis for the 2001 Bhuj earthquake data is carried out on the model.

In the below cases all the displacements are measured with respect to the top most center point of the tank which is also called as crown point.

The following results are obtained from the analysis of the various models.

Table-5: Modal time period and frequencies obtained for empty tank case

| TABLE: Modal Periods And Frequencies |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| OutputCase | StepType | StepNum | Period | Frequency | CircFreq | Eigenvalue |
| Text | Text | Unitless | Sec | Cyc/sec | rad/sec | rad2/sec2 |
| MODAL | Mode | 1 | 0.941105 | 1.06258018 | 6.676388173 | 44.57415904 |
| MODAL | Mode | 2 | 0.941105 | 1.06258018 | 6.676388173 | 44.57415904 |
| MODAL | Mode | 3 | 0.941077 | 1.062612376 | 6.67659047 | 44.57686031 |
| MODAL | Mode | 4 | 0.135709 | 7.368707562 | 46.29895509 | 2143.593242 |
| MODAL | Mode | 5 | 0.135709 | 7.368707562 | 46.29895509 | 2143.593242 |
| MODAL | Mode | 6 | 0.116802 | 8.561464097 | 53.79326542 | 2893.715405 |
| MODAL | Mode | 7 | 0.116728 | 8.566911197 | 53.82749056 | 2897.39874 |
| MODAL | Mode | 8 | 0.106104 | 9.424697116 | 59.21711845 | 3506.667117 |
| MODAL | Mode | 9 | 0.106104 | 9.424697116 | 59.21711845 | 3506.667117 |
| MODAL | Mode | 10 | 0.10229 | 9.776129895 | 61.42523572 | 3773.059583 |
| MODAL | Mode | 11 | 0.089652 | 11.15421481 | 70.08399864 | 4911.766865 |
| MODAL | Mode | 12 | 0.089652 | 11.15421482 | 70.08399864 | 4911.766865 |

Table-6: Base shear and base moments obtained for empty tank for RS (Response spectrum) case

| TABLE: Base Reactions |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OutputCase | CaseType | StepType | StepNum | GlobalfX | Globalfy | Globalfz | GlobalmX | GlobalMY | GlobalMZ |
| Text | Text | Text | Unitless | KN | KN | KN | KN-m | KN-m | KN-m |
| DEAD | LinStatic |  |  | 5.929E-10 | 3.352E-10 | 8551.183 | 45321.2691 | -45321.2691 | -8.036E-10 |
| MODAL | LinModal | Mode | 1 | 1256.376 | 167.673 | -4.328E-07 | -3068.1492 | 22989.6533 | -5770.132 |
| MODAL | LinModal | Mode | 2 | 167.673 | -1256.376 | -1.518E-07 | 22989.6533 | 3068.1492 | -7547.4664 |
| MODAL | LinModal | Mode | 3 | -0.0009594 | 0.0004799 | -4.167E-08 | -0.0088 | -0.0176 | -8715.1706 |
| MODAL | LinModal | Mode | 4 | 4504.998 | -8617.759 | 0.001786 | -209273.217 | -109399.187 | -69550.6075 |
| MODAL | LinModal | Mode | 5 | 8617.756 | 4504.996 | 0.002073 | 109399.1882 | -209273.246 | -21797.6365 |
| MODAL | LinModal | Mode | 6 | $-0.002228$ | -0.001925 | -0.002175 | $-0.0226$ | -0.0216 | -0.0433 |
| MODAL | LinModal | Mode | 7 | $-0.003471$ | 0.005886 | $-0.003713$ | -0.0126 | 0.0174 | 0.0799 |
| MODAL | LinModal | Mode | 8 | -13683.42 | -148.868 | -0.015 | 3284.4315 | -301906.961 | 71733.1188 |
| MODAL | LinModal | Mode | 9 | -148.864 | 13683.42 | 0.03 | -301906.801 | -3284.6855 | 73311.1374 |
| MODAL | LinModal | Mode | 10 | -0.0005491 | -0.002343 | -0.038 | -0.3228 | 0.1555 | -115626.301 |
| MODAL | LinModal | Mode | 11 | -10.286 | 18.121 | -0.003331 | -45.6098 | -25.8366 | 150.5435 |
| MODAL | LinModal | Mode | 12 | -18.112 | -10.277 | 0.05 | 26.4968 | -45.7987 | 41.5933 |
| EQX | LinStatic |  |  | -283.235 | -5.092E-10 | -2.869E-09 | 2.469E-09 | -5487.6917 | 1501.1467 |
| EQY | LinStatic |  |  | -5.239E-10 | -283.235 | -2.051E-09 | 5487.6917 | -6.195E-09 | -1501.1467 |
| RSX | LinRespSpec | Max |  | 283.042 | 0.000002916 | 0.000008925 | 0.00006971 | 5180.2043 | 1500.1209 |
| RSY | LinRespSpec | Max |  | 0.000001782 | 283.042 | 0.00001603 | 5180.2043 | 0.00006409 | 1500.1209 |

Table-7: Displacement of crown point (Joint 35) for empty tank for RS case

| TABLE: Joint Displacements |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Joint | JutputCas | siCaseType | StepTyp | StepNum | U1 | U2 | U3 | R1 | R2 | R3 |
| Text | Text | Text | Text | Unitless | m | m | m | Radians | Radians | Radian |
| 35 | DEAD | Linstatic |  |  | -1.9E-14 | -1E-14 | $-0.00239$ | -9.6E-17 | -6E-17 | -2.2E-1 |
| 35 | MODAL | LinModal | Mode |  | -0.03733 | -0.00498 | -1.4E-12 | 0.000027 | -0.0002 | 3.66E-0 |
| 35 | MODAL | LinModal | Mode | 2 | -0.00498 | 0.037334 | -5.2E-13 | -0.0002 | -2.7E-05 | 2.49E-0 |
| 35 | MODAL | LinModal | Mode | 3 | 2.85E-08 | -1.4E-08 | 2.12E-13 | 7.75E-11 | 1.56E-10 | 0.00522 |
| 35 | MODAL | LinModal | Mode |  | 0.015667 | -0.02997 | 3.29E-09 | 0.004663 | 0.002438 | 1.49E-1 |
| 35 | MODAL | LinModal | Mode | 5 | 0.02997 | 0.015667 | 9.44E-10 | -0.0024 | 0.004663 | -2.5E-1 |
| 35 | MODAL | LinModal | Mode |  | 3.09E-09 | -3.5E-10 | 1.95E-09 | 2.95E-10 | -1.12-08 | -7.3E-1 |
| 35 | MODAL | LinModal | Mode | 7 | -1.3E-09 | 3.59E-09 | 5.13E-09 | 8.05E-09 | 7.29E-09 | 8.01E-1 |
| 35 | MODAL | LinModal | Mode |  | 0.021239 | 0.000231 | 7.22E-09 | -5.9E-05 | 0.005392 | 2.27E-11 |
| 35 | MODAL | LinModal | Mode |  | 0.000231 | $-0.02124$ | -3.2E-09 | 0.005392 | 0.000059 | 2E-11 |
| 35 | MODAL | LinModal | Mode | 10 | 2.53E-10 | -2.7E-09 | 9.31E-09 | -6.9E-09 | -4E-09 | -0.0008 |
| 35 | MODAL | LinModal | Mode | 11 | -3.2E-07 | 5.44E-07 | 1.78E-08 | 2.43E-06 | 1.38E-06 | -4.3E-12 |
| 35 | MODAL | LinModal | Mode | 12 | -5.4E-07 | -3.12-07 | -1.12-07 | -1.45-06 | 2.43E-06 | 2.74E-11 |
| 35 | EQX | Linstatic |  |  | 0.008666 | 1.21E-14 | 6.79E-16 | -1.2E-12 | 0.000051 | -5.5E-1 |
| 35 | EQY | LinStatic |  |  | 2.29E-14 | 0.008666 | 3.63E-16 | -5.1E-05 | -1.2E-12 | 2.75E-1 |
| 35 | RSX | LinRespSF | Max |  | 0.008401 | 2.05E-11 | 4.3E-12 | 6.47E-12 | 0.000046 | 3.8E-1 |
| 35 | RSY | LinRespSF. | Max |  | 2.06E-11 | 0.008401 | 3.3E-12 | 0.000046 | 1.66E-12 | 1.91 E |

Table-8: Base shear and base moments obtained for empty tank for TH (Time History) case

| TABLE: Base Reactions |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OutputCase | CaseType | StepType | StepNum | GlobalFX | Globalfy | Globalfz | GlobalMX | GlobalMY | GlobalMZ |
| Text | Text | Text | Unitless | KN | KN | KN | KN-m | KN-m | KN-m |
| DEAD | LinStatic |  |  | 5.929E-10 | 3.352E-10 | 8551.183 | 45321.2691 | -45321.2691 | -8.036E-10 |
| MODAL | LinModal | Mode | 1 | 1256.376 | 167.673 | -4.328E-07 | -3068.1492 | 22989.6533 | -5770.132 |
| MODAL | LinModal | Mode | 2 | 167.673 | -1256.376 | -1.518E-07 | 22989.6533 | 3068.1492 | -7547.4664 |
| MODAL | LinModal | Mode | 3 | -0.0009594 | 0.0004799 | -4.167E-08 | -0.0088 | -0.0176 | -8715.1706 |
| MODAL | LinModal | Mode | 4 | 4504.998 | -8617.759 | 0.001786 | -209273.217 | -109399.187 | -69550.6075 |
| MODAL | LinModal | Mode | 5 | 8617.756 | 4504.996 | 0.002073 | 109399.1882 | -209273.246 | -21797.6365 |
| MODAL | LinModal | Mode | 6 | -0.002228 | -0.001925 | -0.002175 | -0.0226 | -0.0216 | -0.0433 |
| MODAL | LinModal | Mode | 7 | -0.003471 | 0.005886 | $-0.003713$ | -0.0126 | 0.0174 | 0.0799 |
| MODAL | LinModal | Mode | 8 | -13683.42 | -148.868 | -0.015 | 3284.4315 | -301906.961 | 71733.1188 |
| MODAL | LinModal | Mode | 9 | -148.864 | 13683.42 | 0.03 | -301906.801 | -3284.6855 | 73311.1374 |
| MODAL | LinModal | Mode | 10 | -0.0005491 | -0.002343 | -0.038 | -0.3228 | 0.1555 | -115626.301 |
| MODAL | LinModal | Mode | 11 | -10.286 | 18.121 | -0.003331 | -45.6098 | -25.8366 | 150.5435 |
| MODAL | LinModal | Mode | 12 | -18.112 | -10.277 | 0.05 | 26.4968 | -45.7987 | 41.5933 |
| EQX | LinStatic |  |  | -283.235 | -5.092E-10 | -2.869E-09 | $2.469 \mathrm{E}-09$ | -5487.6917 | 1501.1467 |
| EQY | LinStatic |  |  | -5.239E-10 | -283.235 | -2.051E-09 | 5487.6917 | -6.195E-09 | -1501.1467 |
| THX | NonModHist | Max |  | 283.233 | 0.00000344 | 0.00001295 | 0.0001042 | 5610.606 | 714.3869 |
| THX | NonModHist | Min |  | -134.79 | $-0.000002414$ | $-0.000006307$ | $-0.00004749$ | -2596.6647 | -1501.136 |
| THY | NonModHist | Max |  | 0.000002257 | 283.233 | 0.00002421 | 2596.6648 | 0.00004461 | 1501.1361 |
| THY | NonModHist | Min |  | -0.000001624 | -134.79 | -0.00001111 | -5610.6059 | -0.0000969 | -714.3869 |

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Table-9: Displacement of crown point for empty tank for TH case

| TABLE: Joint Displacements |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Joint | JutputCas | CaseType | StepType | StepNum | U1 | U2 | U3 | R1 | R2 | R3 |
| Text | Text | Text | Text | Unitless | m | m | m | Radians | Radians | Radians |
| 35 | DEAD | LinStatic |  |  | -1.9E-14 | -1E-14 | -0.00239 | -9.6E-17 | -6E-17 | -2.2E-11 |
| 35 | MODAL | LinModal | Mode | 1 | -0.03733 | -0.00498 | -1.4E-12 | 0.000027 | -0.0002 | $3.66 \mathrm{E}-09$ |
| 35 | MODAL | LinModal | Mode | 2 | -0.00498 | 0.037334 | -5.2E-13 | -0.0002 | -2.7E-05 | $2.49 \mathrm{E}-09$ |
| 35 | MODAL | LinModal | Mode | 3 | 2.85E-08 | -1.4E-08 | 2.12E-13 | $7.75 \mathrm{E}-11$ | 1.56E-10 | 0.005227 |
| 35 | MODAL | LinModal | Mode | 4 | 0.015667 | -0.02997 | $3.29 \mathrm{E}-09$ | 0.004663 | 0.002438 | $1.49 \mathrm{E}-13$ |
| 35 | MODAL | LinModal | Mode | 5 | 0.02997 | 0.015667 | 9.44E-10 | $-0.00244$ | 0.004663 | -2.5E-11 |
| 35 | MODAL | LinModal | Mode | 6 | $3.09 \mathrm{E}-09$ | -3.5E-10 | $1.95 \mathrm{E}-09$ | 2.95E-10 | -1.1E-08 | -7.3E-11 |
| 35 | MODAL | LinModal | Mode | 7 | -1.3E-09 | 3.59E-09 | 5.13E-09 | 8.05E-09 | 7.29E-09 | $8.01 \mathrm{E}-11$ |
| 35 | MODAL | LinModal | Mode | 8 | 0.021239 | 0.000231 | 7.22E-09 | -5.9E-05 | 0.005392 | 2.27E-11 |
| 35 | MODAL | LinModal | Mode | 9 | 0.000231 | -0.02124 | -3.2E-09 | 0.005392 | 0.000059 | -2E-11 |
| 35 | MODAL | LinModal | Mode | 10 | $2.53 \mathrm{E}-10$ | -2.7E-09 | 9.31E-09 | -6.9E-09 | -4E-09 | -0.00089 |
| 35 | MODAL | LinModal | Mode | 11 | -3.2E-07 | 5.44E-07 | 1.78E-08 | 2.43E-06 | 1.38E-06 | -4.3E-12 |
| 35 | MODAL | LinModal | Mode | 12 | -5.4E-07 | -3.1E-07 | -1.1E-07 | -1.4E-06 | 2.43E-06 | 2.74E-11 |
| 35 | EQX | LinStatic |  |  | 0.008666 | 1.21E-14 | 6.79E-16 | -1.2E-12 | 0.000051 | -5.5E-14 |
| 35 | EQY | LinStatic |  |  | $2.29 \mathrm{E}-14$ | 0.008666 | 3.63E-16 | -5.1E-05 | -1.2E-12 | 2.75E-14 |
| 35 | THX | NonModH |  |  | 0.004194 | 3.01E-12 | 3.9E-12 | 8.96E-12 | 0.000023 | 1.01E-13 |
| 35 | THX | NonModH | Min |  | -0.00856 | -2.2E-12 | -5.8E-12 | -5.8E-12 | -5.4E-05 | -1.3E-13 |
| 35 | THY | NonModH |  |  | $9.53 \mathrm{E}-13$ | 0.004194 | 2.6E-12 | 0.000054 | 1.02E-12 | 6.74E-14 |
| 135 | THY | NonModH |  |  | -6.9E-13 | -0.00856 | -3.3E-12 | -2.3E-05 | -1.8E-12 | -5.1E-14 |

### 4.2 Full tank condition for fixed base model.

For tank full condition water pressure is applied on the tank wall. Here both impulsive and convective hydrodynamic pressures are calculated and are applied on the wall and base slab of the tank. Proper freeboard should be provided while applying these pressures. Then both response spectrum and time history analysis is carried out for water load and its combinations.

The following results are obtained from the analysis of the various models in Sap 2000


Fig -2: Sectional view of the tank subjected to water pressure

Table-10: Modal time period and frequencies obtained for full tank case

| TABLE: Modal Periods And Frequencies |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| OutputCase | StepType | StepNum | Period | Frequency | CircFreq | Eigenvalue |
| Text | Text | Unitless | Sec | Cyc/sec | rad/sec | rad2/sec2 |
| MODAL | Mode | 1 | 1.548771 | 0.645673081 | 4.056883615 | 16.45830467 |
| MODAL | Mode | 2 | 1.548771 | 0.645673081 | 4.056883615 | 16.45830467 |
| MODAL | Mode | 3 | 1.372201 | 0.728756285 | 4.578910781 | 20.96642394 |
| MODAL | Mode | 4 | 0.169713 | 5.892302659 | 37.02242949 | 1370.660286 |
| MODAL | Mode | 5 | 0.169713 | 5.892302659 | 37.02242949 | 1370.660286 |
| MODAL | Mode | 6 | 0.131567 | 7.600662071 | 47.75636825 | 2280.670708 |
| MODAL | Mode | 7 | 0.116743 | 8.565824576 | 53.82066312 | 2896.663779 |
| MODAL | Mode | 8 | 0.116743 | 8.565824576 | 53.82066312 | 2896.663779 |
| MODAL | Mode | 9 | 0.116612 | 8.575424154 | 53.88097905 | 2903.159903 |
| MODAL | Mode | 10 | 0.11654 | 8.580776059 | 53.91460606 | 2906.784746 |
| MODAL | Mode | 11 | 0.103067 | 9.702417052 | 60.96208426 | 3716.375718 |
| MODAL | Mode | 12 | 0.089573 | 11.16407549 | 70.14595506 | 4920.455011 |

Table-11: Base shear and base moments obtained for full tank for RS (Response spectrum) case

| TABIE: Base Reactions |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OutputCase | CaseType | StepType | StepNum | GlobalfX | Globalfy | Globalfz | GlobalMX | GlobalMY | GlobalMZ |
| Text | Text | Text | Unitless | KN | KN | KN | KN-m | KN-m | KN-m |
| DEAD | LinStatic |  |  | -7.134E-10 | -2.13E-10 | 8551.183 | 45321.2691 | -45321.2691 | 2.395E-09 |
| MODAL | LinModal | Mode | 1 | -747.943 | 122.385 | 0.00001236 | -2158.8335 | -13193.4331 | 4612.7413 |
| MODAL | LinModal | Mode | 2 | -122.385 | -747.943 | 3.165E-08 | 13193.433 | -2158.8336 | -3315.4552 |
| MODAL | LinModal | Mode | 3 | -1.304E-07 | 1.096E-07 | -1.574E-07 | -7.314E-07 | 5.922E-07 | -5908.5515 |
| MODAL | LinModal | Mode | 4 | -2.05 | 3525.431 | $-0.003278$ | 260261.6687 | 151.3234 | 18695.6359 |
| MODAL | LinModal | Mode | 5 | -3525.452 | -2.045 | $-0.001341$ | -151.3252 | 260261.5903 | 18674.0343 |
| MODAL | LinModal | Mode | 6 | 0.006695 | 0.005807 | 104776.278 | 555314.2718 | -555314.19 | 0.0575 |
| MODAL | LinModal | Mode | 7 | -8556.391 | -13370.053 | -0.017 | 115553.3813 | -73950.3374 | -25512.4049 |
| MODAL | LinModal | Mode | 8 | 13370.047 | -8556.404 | 0.009085 | 73950.4603 | 115553.4065 | -116210.261 |
| MODAL | LinModal | Mode | 9 | -0.001806 | -0.003466 | $-0.002809$ | -0.0222 | $-0.0396$ | -0.0258 |
| MODAL | LinModal | Mode | 10 | -0.004554 | $-0.004447$ | 0.003376 | -0.0192 | -0.0645 | -0.0652 |
| MODAL | LinModal | Mode | 11 | -0.004124 | 0.001322 | $-0.009694$ | -0.074 | -0.0559 | 115060.6957 |
| MODAL | LinModal | Mode | 12 | -7.88 | -1.923 | 0.037 | -74.972 | 307.0679 | 31.6349 |
| HYDRO STATIC PRESSURE | LinStatic |  |  | -1.287E-09 | -3.304E-10 | 12876.829 | 68247.1961 | -68247.1961 | 4.679E-09 |
| EQX | LinStatic |  |  | -353.353 | 1.866E-09 | 5.977E-09 | -1.481E-08 | -7818.1304 | 2291.9636 |
| EQY | LinStatic |  |  | 1.874E-09 | -353.353 | 1.635E-09 | 7818.1304 | 3.682E-08 | -2291.9636 |
| RSX | LinRespSpec | Max |  | 351.271 | 0.00001403 | 0.00002185 | 0.00009171 | 7624.6153 | 2291.035 |
| RSY | LinRespSpec | Max |  | 0.000004378 | 351.271 | 0.00001252 | 7624.6153 | 0.00009132 | 2291.035 |

Table-12: Displacement of crown point for full tank for RS case

| Joint | OutputCa: | CaseType | StepType | StepNum | U1 | U2 | U3 | R1 | R2 | R3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Text | Text | Text | Text | Unitless | m | m | m | Radians | Radians | Radians |
| 35 | DEAD | LinStatic |  |  | $2.29 \mathrm{E}-14$ | 6.3E-15 | -0.00254 | -4.5E-16 | -3.4E-17 | -2.3E-11 |
| 35 | MODAL | LinModal | Mode | 1 | 0.022507 | -0.00368 | -7.7E-12 | 0.000018 | 0.000113 | 4.98E-14 |
| 35 | MODAL | LinModal | Mode | 2 | 0.003683 | 0.022507 | 6.06E-14 | -0.00011 | 0.000018 | 3.93E-16 |
| 35 | MODAL | LinModal | Mode | 3 | 7.37E-14 | -5.4E-14 | 6.63E-14 | -5.2E-14 | $6.89 \mathrm{E}-15$ | 0.003585 |
| 35 | MODAL | LinModal | Mode | 4 | -0.00002 | 0.034302 | -1E-08 | -0.00501 | -2.9E-06 | 5.86E-12 |
| 35 | MODAL | LinModal | Mode | 5 | -0.0343 | -0.00002 | -2.8E-08 | $2.91 \mathrm{E}-06$ | -0.00501 | -3.7E-12 |
| 35 | MODAL | LinModal | Mode | 6 | 6.2E-09 | 1.17E-11 | -0.02661 | -4.1E-10 | -2.6E-09 | -1.9E-10 |
| 35 | MODAL | LinModal | Mode | 7 | 0.003754 | 0.005866 | -1.15-09 | -0.00131 | 0.000839 | 6.61E-11 |
| 35 | MODAL | LinModal | Mode | 8 | -0.00587 | 0.003754 | 8.05E-09 | -0.00084 | -0.00131 | 2.84E-11 |
| 35 | MODAL | LinModal | Mode | 9 | -3.1E-09 | 3.65E-10 | -2.1E-08 | -2.1E-09 | -3.1E-09 | 5.95E-12 |
| 35 | MODAL | LinModal | Mode | 10 | -2.3E-09 | $2.43 \mathrm{E}-09$ | $5.71 \mathrm{E}-09$ | -2.1E-09 | -4.7E-09 | 3.66E-11 |
| 35 | MODAL | LinModal | Mode | 11 | -5.5E-09 | 3.51E-10 | -1.8E-08 | -1.2E-09 | $2.48 \mathrm{E}-09$ | 0.000421 |
| 35 | MODAL | LinModal | Mode | 12 | -4.8E-05 | -1.2E-05 | 8.95E-09 | 2.11E-06 | -8.7E-06 | 1.69E-12 |
| 35 | HYDROST | LinStatic |  |  | 4.11E-14 | 9.73E-15 | -0.00276 | -4.9E-16 | 7.81E-17 | -1.2E-13 |
| 35 | EQX | LinStatic |  |  | 0.013156 | -6.4E-14 | -1.2E-15 | -7.7E-13 | 0.000068 | -1.8E-15 |
| 35 | EQY | LinStatic |  |  | -5.7E-14 | 0.013156 | -3.5E-16 | -6.8E-05 | -7.7E-13 | 3.69E-16 |
| 35 | RSX | LinRespSp | Max |  | 0.013 | $2.88 \mathrm{E}-11$ | $2.58 \mathrm{E}-11$ | 5.52E-12 | 0.000065 | 3.5E-14 |
| 35 | RSY | LinRespSp | Max |  | 2.8E-11 | 0.013 | $1.01 \mathrm{E}-11$ | 0.000065 | 5.16E-12 | 6.16E-14 |

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Table-13: Base shear and base moments obtained for full tank for TH (Time History) case

| TABLE: Base Reactions | CaseType | StepIype | StepNum | Globalfx | GlobalFY | GlobalFZ | GlobalMX | GlobalMY | GlobalMZ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OutputCase |  |  |  |  |  |  |  |  |  |
| Text | Text | Text | Unitless | kN | kN | kN | KN-m | KN-m | KN-m |
| DEAD | LinStatic |  |  | -7.134-10 | -2.13E-10 | 8551.183 | 45321.2691 | -45321.2691 | 2.395E-09 |
| MODAL | LinModal | Mode | 1 | -747.43 | 122.385 | 0.00001236 | -2158.8335 | -13193.4331 | 4612.7413 |
| MODAL | LinModal | Mode | 2 | -122.885 | -747.943 | 3.165E-08 | 13193.433 | -2158.8336 | -3315.4552 |
| MODAL | LinModal | Mode | 3 | -1.304E-07 | 1.096E-07 | -1.574E-07 | -7.314E-07 | 5.922E-07 | -5908.5515 |
| MODAL | LinModal | Mode | 4 | -2.05 | 3525.431 | -0.003278 | 260261.6687 | 151.3234 | 18695.6359 |
| MODAL | LinModal | Mode | 5 | -3525.452 | -2.045 | -0.001341 | -151.3252 | 260261.5903 | 18674.0343 |
| MODAL | LinModal | Mode | 6 | 0.006695 | 0.005807 | 104776.278 | 555314.2718 | -555314.19 | 0.0575 |
| MODAL | LinModal | Mode | 7 | -8556.391 | -13370.053 | -0.017 | 115553.3813 | -73950.3374 | -25512.4049 |
| MODAL | LinModal | Mode | 8 | 13370.047 | -8556.404 | 0.009085 | 73950.4603 | 115553.4065 | $-116210.261$ |
| MODAL | LinModal | Mode | 9 | -0.001806 | -0.003466 | -0.002809 | -0.0222 | -0.0396 | -0.0258 |
| MODAL | LinModal | Mode | 10 | -0.004554 | -0.004447 | 0.003376 | -0.0192 | -0.0645 | -0.0652 |
| MODAL | LinModal | Mode | 11 | -0.004124 | 0.001322 | -0.009694 | -0.074 | -0.0559 | 115060.6957 |
| MODAL | LinModal | Mode | 12 | -7.88 | -1.923 | 0.037 | -74.972 | 307.0679 | 31.6349 |
| HYDROSTATIC PRESSURE | LinStatic |  |  | -1.287E-09 | -3.304E-10 | 12876.829 | 68247.1961 | -68247.1961 | 4.679E-09 |
| EQX | LinStatic |  |  | -365.35 | 1.866E-09 | 5.977E-09 | -1.481E-08 | -7818.1304 | 2291.9636 |
| EQY | LinStatic |  |  | 1.874E-09 | -365.35 | 1.635E-09 | 7818.1304 | 3.682E-08 | 2291.9636 |
| THX | NonModHist | Max |  | 364.444 | 0.000009787 | 0.0000352 | 0.0001545 | 7855.5541 | 1371.9744 |
| THX | NonModHist | Min |  | -258.863 | -0.000008836 | -0.00003554 | $-0.0001363$ | -4787.2677 | -2291.9524 |
| THY | NonModHist | Max |  | 0.000004852 | 364.444 | 0.00002072 | 4787.2676 | 0.0001868 | 2291.9524 |
| тНY | NonModHist | Min |  | -0.00000419 | -258,863 | -0.00002393 | -7855.5539 | $-0.0001896$ | -1371.9744 |

Table-14: Displacement of crown point for full tank for TH case

| TABLE: Joint Displacements |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Joint | JutputCasi | CaseType | StepType | StepNum | U1 | U2 | U3 | R1 | R2 | R3 |
| Text | Text | Text | Text | Unitless | m | m | m | Radians | Radians | Radians |
| 35 | MODAL | LinModal | Mode | 1 | 0.022507 | -0.00368 | -7.7E-12 | 0.000018 | 0.000113 | 4.98E-14 |
| 35 | MODAL | LinModal | Mode | 2 | 0.003683 | 0.022507 | 6.06E-14 | -0.00011 | 0.000018 | $3.93 \mathrm{E}-16$ |
| 35 | MODAL | LinModal | Mode | 3 | $7.37 \mathrm{E}-14$ | -5.4E-14 | $6.63 \mathrm{E}-14$ | -5.2E-14 | $6.89 \mathrm{E}-15$ | 0.003585 |
| 35 | MODAL | LinModal | Mode | 4 | -0.00002 | 0.034302 | -1E-08 | -0.00501 | -2.9E-06 | 5.86E-12 |
| 35 | MODAL | LinModal | Mode | 5 | -0.0343 | -0.00002 | -2.8E-08 | 2.91E-06 | -0.00501 | -3.7E-12 |
| 35 | MODAL | LinModal | Mode | 6 | 6.2E-09 | 1.17E-11 | -0.02661 | -4.1E-10 | -2.6E-09 | -1.9E-10 |
| 35 | MODAL | LinModal | Mode | 7 | 0.003754 | 0.005866 | -1.1E-09 | -0.00131 | 0.000839 | 6.61E-11 |
| 35 | MODAL | LinModal | Mode | 8 | -0.00587 | 0.003754 | 8.05E-09 | -0.00084 | -0.00131 | $2.84 \mathrm{E}-11$ |
| 35 | MODAL | LinModal | Mode | 9 | -3.1E-09 | $3.65 \mathrm{E}-10$ | -2.1E-08 | -2.1E-09 | -3.1E-09 | 5.95E-12 |
| 35 | MODAL | LinModal | Mode | 10 | -2.3E-09 | $2.43 \mathrm{E}-09$ | 5.71E-09 | -2.1E-09 | -4.7E-09 | 3.66E-11 |
| 35 | MODAL | LinModal | Mode | 11 | -5.5E-09 | 3.51E-10 | -1.8E-08 | -1.2E-09 | $2.48 \mathrm{E}-09$ | 0.000421 |
| 35 | MODAL | LinModal | Mode | 12 | -4.8E-05 | -1.2E-05 | 8.95E-09 | 2.11E-06 | -8.7E-06 | 1.69E-12 |
| 35 | HYDRO ST. | LinStatic |  |  | 4.11E-14 | 9.73E-15 | -0.00276 | -4.9E-16 | 7.81E-17 | -1.2E-13 |
| 35 | EQX | LinStatic |  |  | 0.013156 | -6.4E-14 | -1.2E-15 | -7.7E-13 | 0.000068 | -1.8E-15 |
| 35 | EQY | LinStatic |  |  | -5.7E-14 | 0.013156 | -3.5E-16 | -6.8E-05 | -7.7E-13 | 3.69E-16 |
| 35 | THX | NonModH | Max |  | 0.008047 | 9.46E-12 | 2.68E-11 | 4.96E-12 | 0.000042 | 1.99E-14 |
| 35 | THX | NonModH | Min |  | -0.01341 | -6.4E-12 | -3.1E-11 | -5.6E-12 | -6.8E-05 | -4E-14 |
| 35 | THY | NonModH | Max |  | $9.36 \mathrm{E}-12$ | 0.008047 | 1.03E-11 | 0.000068 | 9.21E-12 | 1.19E-13 |
| 135 | THY | NonModH | Min |  | -7E-12 | -0.01341 | -1.4E-11 | -4.2E-05 | -7.7E-12 | -1E-13 |

### 4.3 Soil structure interaction



Fig -3: Intze tank with soil model

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Table-17: Displacement of crown point for empty tank for SSI case

| Joint | OutputCa | CaseType | StepType | StepNum |  | U2 | U3 | R1 | R2 | R3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Text | Text | Text | Text | Unitless | m | m | m | Radians | Radians | Radians |
| 35 | DEAD | LinStatic |  |  | -1.3E-11 | -1.2E-11 | -0.27321 | 3.02E-13 | -3.3E-13 | -2.2E-11 |
| 35 | MODAL | LinModal | Mode | 1 | 0.04008 | 0.007963 | -1.4E-10 | -0.00021 | 0.001049 | 6.24E-12 |
| 35 | MODAL | LinModal | Mode | 2 | $-0.00796$ | 0.04008 | -8E-11 | -0.00105 | -0.00021 | 1.51E-12 |
| 35 | MODAL | LinModal | Mode | 3 | 0.006771 | 0.002832 | -3.2E-09 | -3.2E-05 | 0.000077 | 7.83E-11 |
| 35 | MODAL | LinModal | Mode | 4 | 0.002832 | -0.00677 | -3.9E-09 | 0.000077 | 0.000032 | 1.62E-10 |
| 35 | MODAL | LinModal | Mode | 5 | $1.31 \mathrm{E}-09$ | $9.11 \mathrm{E}-09$ | $1.93 \mathrm{E}-09$ | -1.2E-09 | -8.7E-10 | -0.00402 |
| 35 | MODAL | LinModal | Mode | 6 | $4.69 \mathrm{E}-09$ | 7.07E-09 | 5.45E-09 | -4E-10 | -6.7E-10 | -3.8E-10 |
| 35 | MODAL | LinModal | Mode | 7 | -1.3E-10 | -7.8E-10 | -7.1E-09 | -3.1E-10 | 5.78E-10 | -0.00327 |
| 35 | MODAL | LinModal | Mode | 8 | -1.6E-09 | -4.5E-09 | -0.0057 | $2.53 \mathrm{E}-10$ | 7.77E-10 | 3.18E-10 |
| 35 | MODAL | LinModal | Mode | 9 | -1.8E-09 | 6.15E-09 | $-0.00674$ | -1.7E-09 | -1.7E-09 | -5.4E-10 |
| 35 | MODAL | LinModal | Mode | 10 | -2.9E-09 | -7.5E-09 | $-5.3 \mathrm{E}-09$ | 1.97E-09 | 6.48E-10 | 1.99E-09 |
| 35 | MODAL | LinModal | Mode | 11 | -0.0031 | -0.00087 | 1.76E-09 | 0.000088 | -0.00031 | -5.5E-11 |
| 35 | MODAL | LinModal | Mode | 12 | -0.00087 | 0.003101 | -3.7E-10 | -0.00031 | -8.8E-05 | -2.7E-09 |
| 35 | RSX | LinRespSp | Max |  | 0.026295 | 1.36E-08 | $4.62 \mathrm{E}-08$ | $2.49 \mathrm{E}-09$ | 0.00094 | $1.61 \mathrm{E}-08$ |
| 35 | RSY | LinRespSp | Max |  | $1.36 \mathrm{E}-08$ | 0.026295 | 3.95E-08 | 0.00094 | 6.6E-09 | $1.68 \mathrm{E}-08$ |
| 35 | EQX | LinStatic |  |  | 0.210008 | $2.14 \mathrm{E}-12$ | $2.86 \mathrm{E}-13$ | -7E-12 | 0.004818 | -1.2E-12 |
| 35 | EQY | LinStatic |  |  | $2.07 \mathrm{E}-12$ | 0.210008 | 2.6E-13 | -0.00482 | -6.9E-12 | 5.11E-13 |
| 35 | THX | NonModH | Max |  | 0.016658 | $2.21 \mathrm{E}-08$ | 4.29E-08 | 2.3E-09 | 0.000964 | 1.31E-08 |
| 35 | THX | NonModH | Min |  | -0.02934 | -1.1E-08 | -5E-08 | -3.3E-09 | $-0.00119$ | -1.7E-08 |
| 35 | THY | NonModH | Max |  | 6.86E-09 | 0.016658 | 4.51E-08 | 0.00119 | 7.08E-09 | 1.54E-08 |

Table-18: Modal period and frequencies for full tank during SSI analysis

| TABLE: Modal Periods And Frequencies |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| OutputCase | StepType | StepNum | Period | Frequency | CircFreq | Eigenvalue (

Table-19: Base shear and Base moment for full tank for SSI analysis

| TABLE: Base Reactions |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OutputCase | Casetype | StepType | StepNum | Globalfx | Globalfy | Globalif | GlobalMX | GlobalMY | GlobalMZ |
| Text | Text | Text | Unitless | kN | kN | kN | kN-m | kN-m | kN-m |
| DEAD | LinStatic |  |  | -6.347E-08 | 2.113E-08 | 106476.809 | 56431.61 | -56432 | 4.39E-07 |
| MODAL | LinModal | Mode | 1 | 164.399 | -164.401 | 0.29 | 1657.1325 | 1657.0666 | -1742.6307 |
| MODAL | LinModal | Mode | 2 | 163.711 | 163.71 | 0.00009082 | -1672.0277 | 16721.0212 | -14.5001 |
| MODAL | LinModal | Mode | 3 | -3221.861 | 3221.863 | -1.495 | 12797.729 | 127989.497 | 3415.667 |
| MODAL | LinModal | Mode | 4 | 3224.495 | 3224.503 | -7.734E-05 | 12797.9608 | -127974.83 | -470.3571 |
| MODAL | LinModal | Mode | 5 | 16.169 | 16.169 | 0.0006137 | 637.2829 | -637.2632 | 11722.6136 |
| MODAL | LinModal | Mode | 6 | -5.165 | 5.165 | 2.944 | 163.4765 | 132.4092 | 54.6674 |
| MODAL | LinModal | Mode | 7 | 1.561 | 1.571 | 0.003596 | 91.9069 | -91.7829 | -15466.352 |
| MODAL | LinModal | Mode | 8 | -1.515 | 1.542 | 14279.698 | 7571.0573 | -75646.483 | 16.1851 |
| MODAL | LinModal | Mode | 9 | 5.108 | -5.126 | 2531.755 | 1331.4061 | -13519.886 | -53.8886 |
| MODAL | LinModal | Mode | 10 | -28.316 | -28.217 | 0.004597 | 18.501 | -17.1782 | 9.1681 |
| MODAL | LinModal | Mode | 11 | 8840.551 | -8840.492 | 0.424 | -804.6099 | -809.9075 | -9370.08 |
| MODAL | LinModal | Mode | 12 | 8837.717 | 8837.731 | 0.004214 | 774.5428 | -774.5021 | -16.4042 |
| HYORO STATIC PRESSURE | LinStatic |  |  | -9.021E-09 | 3.0311-09 | 12876.829 | 68247.1961 | -68247.196 | 6.134E-08 |
| EQX | LinStatic |  |  | -417.396 | 1.055E-08 | 5.515E-08 | -1.568E-07 | 12634.2846 | 22110.3332 |
| EQY | LinStatic |  |  | 1.109E-08 | -417.396 | -1.931-08 | -12634.285 | 5.596E-07 | -22111.262 |
| RSX | LinRespSpec | Max |  | 405.44 | 20.943 | 7.648 | 652.3358 | 11352.0666 | 21481.7971 |
| RSY | LinRespSpec | Max |  | 20.965 | 405.348 | 7.635 | 11352.16 | 663.354 | 21480.6882 |
| THX | NonModhist | Max |  | 411.957 | 68.4 | 190.298 | 1689.3844 | 11384.52 | 69293.38 |
| THX | NonModHist | Min |  | -393.309 | -63.5 | -191.029 | -1772.4315 | -11455.5 | -61988.3 |
| THY | NonModHist | Max |  | 68.115 | 411.722 | 190.739 | 11656.6 | 1822.7603 | 62036.75 |
| THY | NonModhist | Min |  | -63.401 | -393.309 | -189.803 | -1438 | -1673.1083 | -69247.6 |

Table-20: Displacement of crown point for full tank for SSI case

| TABLE: Joint Displacements |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Joint | JutputCas | CaseType | StepType | StepNum | U1 | U2 | U3 | R1 | R2 | R3 |
| Text | Text | Text | Text | Unitless | m | m | m | Radians | Radians | Radians |
| 35 | DEAD | LinStatic |  |  | -0.00019 | 0.000187 | -0.27337 | -6.7E-06 | -6.7E-06 | -2.3E-11 |
| 35 | MODAL | LinModal | Mode | 1 | -0.02893 | 0.028926 | -1.5E-05 | $-0.00076$ | $-0.00076$ | 3.64E-12 |
| 35 | MODAL | LinModal | Mode | 2 | -0.02891 | -0.02891 | 5.3E-10 | 0.000757 | -0.00076 | 5.24E-06 |
| 35 | MODAL | LinModal | Mode | 3 | 0.00515 | $-0.00515$ | 9.68E-06 | 0.000059 | 0.000059 | 1.75E-10 |
| 35 | MODAL | LinModal | Mode | 4 | -0.00519 | $-0.00519$ | 3.86E-09 | 0.000059 | -5.9E-05 | 0.000022 |
| 35 | MODAL | LinModal | Mode | 5 | -6.1E-05 | -6.1E-05 | 4.21E-09 | $2.14 \mathrm{E}-06$ | -2.1E-06 | $-0.00396$ |
| 35 | MODAL | LinModal | Mode | 6 | 0.000027 | -2.7E-05 | -8.9E-06 | 3.06E-07 | 3.07E-07 | $2.16 \mathrm{E}-10$ |
| 35 | MODAL | LinModal | Mode | 7 | -2.6E-05 | -2.6E-05 | 5.86E-09 | 1.4E-06 | -1.4E-06 | -0.00337 |
| 35 | MODAL | LinModal | Mode | 8 | 6.72E-06 | -6.7E-06 | -0.00571 | $2.67 \mathrm{E}-08$ | $2.74 \mathrm{E}-08$ | 5.49E-11 |
| 35 | MODAL | LinModal | Mode | 9 | -2.8E-05 | 0.000028 | 0.00675 | -3.2E-08 | -3.2E-08 | -5E-10 |
| 35 | MODAL | LinModal | Mode | 10 | -2.6E-05 | -2.6E-05 | 1.46E-08 | 2.3E-06 | -2.3E-06 | 9.68E-06 |
| 35 | MODAL | LinModal | Mode | 11 | 0.002281 | -0.00228 | 3.02E-06 | 0.000231 | 0.000231 | -5.9E-10 |
| 35 | MODAL | LinModal | Mode | 12 | 0.00229 | 0.00229 | -4.7E-09 | -0.00023 | 0.000231 | -3.1E-06 |
| 35 | HYDROS | LinStatic |  |  | -0.00032 | 0.000321 | -0.03924 | -1.2E-05 | -1.2E-05 | -1.2E-13 |
| 35 | EQX | LinStatic |  |  | 0.210329 | -0.00045 | 0.000045 | 0.000018 | 0.004835 | -1.3E-05 |
| 35 | EQY | LinStatic |  |  | -0.00045 | 0.210329 | -4.5E-05 | -0.00484 | -1.8E-05 | -1.3E-05 |
| 35 | RSX | LinRespSp | Max |  | 0.03108 | 0.000306 | 0.000025 | 7.93E-06 | 0.001112 | 0.000016 |
| 35 | RSY | LinRespSp | Max |  | 0.000306 | 0.03108 | 0.000025 | 0.001112 | 7.93E-06 | 0.000016 |
| 35 | THX | NonModH |  |  | 0.771181 | 0.004948 | 0.000781 | 0.000122 | 0.030674 | 0.000489 |
| 135 | THX | NonModH |  |  | -0.73249 | $-0.00472$ | -0.0007 | -0.00012 | $-0.02705$ | -0.00053 |

## 6. CONCLUSIONS

Base shear and base moment in full condition tank is slightly higher than empty tank due to absence of water pressure. By providing the free board height of 1.8 m which is greater than the sloshing wave height of 0.386 m we can reduce the additional stresses coming on the top dome.Since total base shear ( 347.33 kN ) and base moment ( $7354.75 \mathrm{kN}-\mathrm{m}$ ) in tank full condition are more than that total base shear ( 234.592 kN ) and base moment ( $4683.261 \mathrm{kN}-\mathrm{m}$ ) in tank empty condition, design will be governed by tank full condition.

For the applied Bhuj earthquake data maximum displacement of the crown point in case of soil structure model is found to be around 770 mm at 44.40 sec for tank full condition and around 650 mm at 44.40 sec for empty condition. The additional deflection in tank full condition is due to hydrodynamic pressure induced in the structure due to sloshing effect.

The maximum hydrodynamic pressure obtained is 2.708 $\mathrm{kN} / \mathrm{m} 2$ which is about $3 \%$ of hydrostatic pressure at base ( $\rho$ $\mathrm{gh}=1,000 \times 9.81 \times 7.0=68 \mathrm{kN} / \mathrm{m}^{2}$ ). In practice, container of tank is designed by working stress method. When earthquake forces are considered, permissible stresses are increased by $33 \%$. Hence, hydrodynamic pressure in this case does not affect container design.

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