Abstract —This paper presents a new interleaved high step-up DC-DC converter is proposed for distributed generation systems. That combines coupled-inductor and switched-capacitor, the proposed converter achieves very high step-up voltage gain without high turns ratio. High boost dc-dc converters play an important role in renewable energy sources such as fuel energy systems, DC-buck energy systems for UPS, high-intensity discharge lamps and automobile applications. Current stress and input current ripple also reduced by the alignment of the proposed converter, The coupled inductors can be designed to extend step-up gain, and the switched capacitors offer extra voltage conversion ratio and the efficiency is improved. The high step-up conversion may require two-stage converters with cascade structure for enough step-up gain, which decreases the efficiency and increases the cost. Thus, a high step-up converter is seen as an important stage in the system. A prototype with the input voltage developed by more than 10 times to verify the theoretical analysis.

Key Words: interleaved, Coupled inductor, high step-up converter, voltage multiplier module, voltage booster.

1. INTRODUCTION

Distributed generation (DG) systems have attracted substantial observation in recent years. The integration of renewable energy into DG systems is becoming increasingly important. The renewable sources, such as Wind energy, thermoelectric cooling(Peltier), Microbial Fuel Cells. Generate low output voltage, typically 20V-40V. Such low-level voltage needs to be boosted to a high DC-bus voltage (380V or 400V) for grid connection[1]-[2]. Therefore, a high step-up dc-dc converter with high efficiency is required in these systems. The conventional boost converter is not suitable for high step-up applications due to the extreme duty-cycle operation, which results in high power losses. Various boosting techniques have been proposed to achieve high step-up conversion[5]. Switched capacitor (SC), also known as voltage multiplier (VM) or charge pump, is one approach to extend the voltage gain. Step-up converters combining the boost-type structure with Cockcroft–Walton (CW) multiplier, Dickson multiplier, voltage doublers or other diode-capacitor cells have been introduced in the literature[6], extended by increasing the number of cells. However, a large number of diodes and capacitors are needed in high step-up applications, which increases the cost and degrades the efficiency. Besides, these topologies may suffer from diode reverse recovery and EMI problems. Additional components may be needed to handle this issue.

Utilizing magnetic coupling provides an extra degree of freedom for high step-up converters [7]. Voltage gain can be extended by increasing the turns ratios. However, the leakage inductance of the coupled inductor or the transformer may result in large voltage spikes across the switches, which causes high voltage stress and degraded efficiency. As a result, converters with passive or active clamp were proposed to handle the leakage problem. In applications requiring a very high conversion ratio, these converters have to use high turns ratio to obtain a large voltage gain. High turns ratio can reduce the efficiency and increase the size of the magnetic [8]. Also, it may result in a very large current ripple. Integrating coupled inductor and switched capacitor is an attractive approach for high step-up converters. Voltage gain is extended by both the turns ratio and the switched capacitor cells. Meanwhile, leakage energy can be recycled with the aid of the switched capacitor cells and diode reverse recovery can be alleviated by the leakage inductance. Due to the single-phase structure, the coupled inductor causes pulsating input current. Thereby, an input filter is needed, which increases the size and cost. Interleaving techniques can be employed to minimize current ripple, reduce the size of magnetic, and increase the current level. Interleaved high step-up converters were proposed by integrating the interleaved boost converter with VM modules[10]. High voltage gain, low switch voltage stress, and low input current ripple can be achieved. In a converter combining modified interleaved boost and VM module was proposed. A converter integrating coupled inductors with two voltage-double modules was proposed. These two converters also utilizes input-parallel and output-series connection to reduce the current ripple and extend the voltage gain. But they do not have a common ground between the input and the output. A three-state switching converter mixed with magnetic coupling and VM module was proposed in. Unfortunately, the currents through the two coupled inductors are not balanced. An interleaved high step-up converter with an active clamp circuit was proposed in Zero-voltage switching of the switches and zero-current.
2. BLOCK DIAGRAM

2.1 THERMAL POWER PRODUCTION

A Peltier module is a semiconductor-based electronic component. The temperature differential of the two sides of the module is used to generate electricity. Fig-1 shows the Peltier module. By applying a low voltage DC power to the module from one side to the other. One face will be cooled while the opposite face it simultaneously heated. That this phenomenon may be reversed. By chance in the polarity of the applied DC voltage will cause heat to be moved in the opposite direction. Consequently, both heating and cooling operations are possible thereby making it highly suitable for precise temperature control applications.

Fig-1: Peltier module

2.2 POWER PRODUCTION FROM WASTEWATER BY USING MICROBIAL FUEL CELLS (Fig2)

A microbial fuel cell is a power-producing device that converts chemical energy into electrical energy. The action of microorganisms is used to produce electricity. It is a bio-electrochemical system. That uses bacteria as the catalyst to oxidize organic and inorganic matter. An electrode is placed in the wastewater. Generally, Bacteria grow on it. These bacteria are transforming the organic compounds present in the water into electricity. The wastewater is purified by this process, which is one useful application. Bio-catholyte had also lower internal resistance, and it improved the current generation; maximum COD removal and desalination rate were 80% and 0.38 g NaCl L−1 h−1, respectively. On the removal and desalination rate were 73.1% and 0.34 g NaCl L−1 h−1 respectively.

Fig-2: Microbial Fuel Cells

2.3 POWER PRODUCTION FROM WIND ENERGY

Wind turbines convert the kinetic energy from the rotation of the turbine by the wind flow into mechanical power. This mechanical power can be used for specific tasks generator can convert this mechanical power into electricity to power homes, businesses, schools. Fig-3 shows small-scale wind turbines. The small-scale wind turbines are used to power generation at a household level. A small-scale wind turbine consists of an agenator, a power electronic converter, and a control system. And permanent magnet (PM) generator is widely used because of its high reliability and simple structure. depends on the required output power and cost of the system. The power electronic converter topology used.

Fig-3: wind turbine

2.4 PIC 16F877A MICROCONTROLLER

It is a High-performance RISC CPU. TO learn All single-cycle instructions except for program branches which are two-cycle. Operating speed: DC - 20 MHz clock input DC - 200 ns instruction cycle. Up to 8K x 14 words of FLASH Program Memory, Up to 368 x 8 bytes of Data Memory (RAM). Up to 256 x 8 bytes of EEPROM Data Memory.
3. ENTIRE CIRCUIT DIAGRAM

The generalized structure of the proposed converter is shown in Fig-4. It is composed voltage multiplier circuit, three energy sources (wind, Peltier, microbial fuel cells) and one output monitor. In the voltage multiplier circuit, The primary windings of the coupled inductors are connected in parallel and the secondary windings are connected in series. Both coupled inductors are modeled as an ideal transformer with magnetizing inductance and leakage inductance. The two switches of the proposed converter are driven in an interleaved manner. The structure of the proposed converter is shown in Fig-6. It comprises an interleaved voltage-doubler boost converter and multiple winding-based switched capacitor (WSC) cells. Each WSC cell has two diodes, two capacitors and two windings of the coupled inductors. Fig-7 shows the basic topology with one WSC cell. It is composed of two coupled inductors, two switches, four diodes, three energy transfer capacitors, and one output capacitor. The primary windings of the coupled inductors are connected in parallel and the secondary windings are connected in series. The turns ratios of the coupled inductors are the same.

The below Fig-7 shows the voltage multiplier circuit. which is used to boost up the voltage from given 12 volt to 350 volt. The duty cycle D during steady-state is larger than 0.5. In this paper, the operation in continuous conduction mode (CCM) is discussed.

The equivalent circuit of the proposed converter is shown below Fig-8. where Lm1 and Lm2 are the magnetizing inductors; Lk1 and Lk2 represent the leakage inductors; Ls represents the series leakage inductors in the secondary side; S1 and S2 denote the power switches; Cc1 and Cc2 are the switched capacitors; and C1, C2, and C3 are the output capacitors.
4. MODES OF OPERATIONS

According to the operation of S1 and S2, there are eight operating modes when operates in the continuous conduction mode (CCM). Fig.9 represents several key waveforms of one cycle. And Fig-10 represents the equivalent circuit of the converter in different modes.

Mode I \([t_0 \sim t_1]\): At the time of \(t_0\), S1 is switched on, the S2 maintains the state of conducting. Because the current of the inductor can’t be changed suddenly, the diode D4 is still on. The current through the diode D4 decreases gradually. When the \(i_D4\) is reduced to zero, D4 is turned off under ZCS.

Mode II \([t_1 \sim t_2]\): At the time of \(t_1\), S1 and S2 are switched on. All diodes are reverse biased. During this transition, \(L_{m1}, L_{m2}, L_{k1}\), and \(L_{k2}\) are charged linearly by the input power. The energy of load is provided by the two output capacitors.

Mode III \([t_2 \sim t_3]\): At the time of \(t_2\), the S2 is switched off, S1 maintains the state of conducting. Diodes D1 and D3 are on. Part of the energy stored in \(L_{k2}\) is transferred to \(C_1\) via D1. The input voltage, coupled-inductors, and \(V_{C2}\) are in series to charge the capacitor C4, extending the voltage gain of this converter. The current \(I_{Lk2}\) begins to decrease. At the same time, the current \(I_{D1}\) is decreased gradually. D1 is turned off under the ZCS condition.

Mode IV \([t_3 \sim t_4]\): At the time of \(t_3\), D1 is turned off, as shown in Fig. 2(d). \(L_{m1}\) and \(L_{k1}\) are charged linearly by the input dc source. C4 is still charged through \(L_{m2}, L_{k2}\), and \(C_2\). The load current is provided by \(C_3\). In this mode, S1 and S2 are switched on. The energy of load is provided by the capacitors \(C_3\) and \(C_4\).

Mode VII \([t_6 \sim t_7]\): At the time of \(t_6\), the S1 is switched off and \(S_2\) continues to be turned on. Diodes \(D_2\) and \(D_4\) are turned on. Part of the energy stored in \(L_{k1}\) is transferred to \(C_2\) via \(D_2\). The leakage inductor energy is reclaimed by \(C_2\), which can be used to reduce the losses. Another part of the energy stored in \(L_{k1}\) and the energy stored in \(C_1\) are transferred to \(C_3\) via \(D_4\). The current \(I_{Lk1}\) begins to decrease. At the same time, the current \(I_{D2}\) is decreased gradually. The current of \(D_2\) drops to zero and it is turned off under ZCS, and this mode ends.

Mode VIII \([t_7 \sim t_8]\): At the time of \(t_7\), D2 is turned off. In this mode, \(L_{m2}\) and \(L_{k2}\) are charged linearly by the input voltage. \(C_3\) is charged by \(L_{m1}, L_{k1}\), and \(C_1\).

4.1. VOLTAGE CONVERSION CIRCUIT

Therefore the input voltage ranging from \(v_{in}=0-20v\) is scaled down to the output \(v_a=0-5v\).

5. EXPERIMENTAL RESULTS

A prototype with 12V input and 350V output was built to verify the performance of the proposed converter. The key parameters of the prototype are listed as in Table1. A picture of the prototype is shown in Fig.10.

Fig.11 shows that the input voltage is 20V and the output voltage is 400V. Therefore, high voltage gain is achieved even when the turns ratio is 1.

Fig.12 shows the voltages of the diodes. As can be seen, the blocking voltages of \(D_1\) and \(D_2\) are around 136V and the blocking voltages of \(D_1\) and \(D_2\) are around 268V.

Fig.13 shows the currents through the diodes. It can be seen that the reverse recovery problems of the diodes are alleviated due to the existence of the leakage inductances.

**Table1:** key parameters of the prototype

<table>
<thead>
<tr>
<th>parameters</th>
<th>Value/description</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input voltage</td>
<td>20V</td>
</tr>
<tr>
<td>Output voltage</td>
<td>400V</td>
</tr>
<tr>
<td>power</td>
<td>320W</td>
</tr>
<tr>
<td>Switching frequency</td>
<td>50kHz</td>
</tr>
<tr>
<td>Switches S1-S2</td>
<td>IPA075N15N3 (150V)</td>
</tr>
<tr>
<td>Diodes D1, D2</td>
<td>STPS20200CT (200V)</td>
</tr>
<tr>
<td>Diodes D3, D4</td>
<td>TST20H300CW(300V)</td>
</tr>
<tr>
<td>Coupled inductors</td>
<td>Magnetizing inductance = 100uH Leakage inductance = 3.5uH</td>
</tr>
</tbody>
</table>
Capacitor $C_1$ | 22uF Film capacitor  
Capacitor $C_2, C_3$ | 8.2uF Film capacitor  
Capacitor $C_0$ | 256uF electrolytic capacitor

Fig.10: picture of the prototype

Fig.11: The input and output voltages

Fig.12: Voltages across the diodes

Fig.13: current across the diode

Fig.14: Voltages across the capacitors.

### 6. CONCLUSION

An interleaved high step-up converter integrating coupled-inductor and switched-capacitor techniques has been proposed in this paper. It is shown that very high step-up voltage gain is achieved without an extreme duty cycle or high turns ratio. Also, due to the low switch voltage stress, low-voltage-rating MOSFETs with small on-resistance are allowed to reduce the conduction loss. Furthermore, low-ripple continuous input current is achieved thanks to the interleaved operation at the input side. Moreover, ZCS turn-on of the switches is achieved and the reverse recovery problem of the diodes is alleviated. Also, the leakage energy is recycled. The operation principles and characteristics of the basic topology were analyzed in detail. A 20V-input and 400V-output prototype was built. Experimental results have verified the theoretical analysis.

### REFERENCES


