PERFORMANCE ANALYSIS OF THE GRID - SIDE CONVERTER CONTROL SYSTEM FOR THE GRID - CONNECTED SYNCHRONOUS GENERATOR WIND TURBINES

Sujit Kumar Sah
Former PG Scholar at National Institute Of Technology, Nagaland

Abstract - This paper describes the performance analysis of the grid side converter (GSC) control system of a variable speed wind turbine (VSWT) which is driven by a synchronous generator. It is connected to the grid using a fully controlled converter. It consists of a rectifier, an intermediate dc circuit, and a PWM inverter through a filter. The main objective of this system is to achieve high power quality, low distortion and large power export from the converter. Control systems are put into for regulating dc voltage for various input conditions, for regulating the grid current entering the distribution network and hence power flow into the grid. Steady state and dynamic performance analysis of the converter control system under different conditions are investigated.

Key Words: GSC, VSWT, Synchronous Generator, PWM inverter, Filter.

1. INTRODUCTION

With the increasing demand of electricity, the use of fossil fuel is getting increased very rapidly in present world. All living and non-living beings including the environment is severely affected continuously because of the use of it. To overcome these consequences, the wind energy conversion system for electricity generation is very advantageous over conventional fossil fuel energy resources. It is safe, pollution free and inexhaustible sources of energy. A capacity addition of 27.07 GW of renewable energy has been reported during the last three and half years under Grid Connected Renewable Power, which include 11.70 GW from Wind Power [13].

The kinetic energy which is available in the wind is converted into mechanical energy with the help of a turbine. The synchronous generator converts this mechanical energy into electrical energy. Then generator side PWM converter convert this AC power into DC power, grid side converter convert this DC power into AC power which is fed to the grid. As we know that the wind is intermittent in nature, than the wind extracted by a wind turbine is not constant. The fluctuation of wind power results in fluctuated power output from wind turbine generator. Because of the fluctuation of generator output power, it’s not suitable for the generator to be directly connected to the power grid. To feed the generator output power to the grid, it is very important to use a grid side converter controller for synchronization.

Fig -1: Block diagram of the wind energy conversion system

1.1 GRID SIDE CONVERTER CONTROL SYSTEM

The main reason for the Grid Side, Converter Control system is to modulate the inverter for adjusting the phase angle and the magnitude of the grid supply current so that the power which is entering the network can be controlled. The measured three phase ac currents are transformed into dc components for removing the steady state error. Besides it has also the advantage of controlling the real and reactive power independently. The reference grid currents in the dq axis are obtained from the active and reactive power reference set points. These reference currents need to be synchronized to the grid voltage.

Fig -2: Block diagram of Grid Side Converter Control using FOC Algorithm [1]
Fig-2 shows the control strategy which is used for the generation of reference currents. PI control scheme is used for the control of both active and reactive power flow into the grid. The active power control is done through the d-axis component of grid current and the reactive power control through the q-axis component of grid current. The d and q axis reference currents are calculated as per the equations 1 and 2 as shown below. The three phase grid currents I_a, I_b and I_c are sensed and transformed to dq0 reference frame. Synchronization of the reference frame to the grid voltage is achieved by Phase Locked Loop (PLL) method [1]. The control voltages for the three phases Voltage Source Inverter are generated based on the errors in d axis and q axis currents through PI controllers. The PI controllers produce the control voltages for the inverter in d and q axis based on equations 3 and 4. The compensation terms are added to improve the transient response of the system.

\[
I_d(\text{ref}) = K_p V_h + K_i \int V_h \, dt \quad (1)
\]

\[
I_q(\text{ref}) = K_p V_j + K_i \int V_j \, dt \quad (2)
\]

\[
V'_d = K_p I_h + K_i \int I_h \, dt \quad (3)
\]

\[
V'_q = K_p I_j + K_i \int I_j \, dt \quad (4)
\]

Where \( I_h \) and \( I_j \) are the errors in d axis and q axis grid currents and \( K_p, K_i \) are the proportional and integral gains of the PI controllers. The voltages \( V'_d, V'_q \) are then transformed into a b c coordinates to get control voltages \( V_a, V_b \) and \( V_c \) for the PWM inverter.

2. SIMULATION AND PERFORMANCE EVALUATION

To evaluate the performance of the system, the model is examined under various conditions. These conditions include steady-state and dynamic conditions analysis such as variation in grid voltage and fault conditions. In each case, the performance of the system is analyzed. DC link voltage is maintained constant; the minimum value of dc reference voltage is determined by the inverter output voltage as

\[ V_{dc\,(\text{ref})} = 2 \times \frac{2}{\sqrt{3}} V_{g\text{-line}} \]

where \( V_{g\text{-line}} \) is the line to line voltage at the inverter output.

Fig-3 shows the steady-state analysis of the system in which we can see that the system reaches steady-state after 2.5s.

Fig-4 shows the effect on the system when 25% dip in grid voltage occurs between 4.5s to 5.5s. Active power reference is set at 2 MW and reactive power reference is set at zero. During the voltage dip, distortion in grid current occurs, and thus distortions are seen in active and reactive power. When distortion in grid voltage is cleared the active and reactive power follow the respective references. It also shows the effect on dc link voltage and voltage and current at the point of common coupling.
Fig-5: Dynamic analysis of the system for 25% rise in grid voltage.

Fig-5 shows the effect on the system when 25% rise in grid voltage imposed between time t= 4.5s and cleared at t= 5.5s. Active power reference is set at 2 MW and reactive power reference is set at zero. During the voltage rise, distortion in grid current occurs, and thus distortions are seen in active and reactive power. When distortion in grid voltage is cleared the active and reactive power follow the respective references. It also shows the effect on dc link voltage and voltage and current at the point of common coupling.

Fig-6: Response of the system under the single line to a ground fault condition.

Fig-6 shows the response of the system the under single line to a ground fault condition. Fault occurs at t = 4s and cleared at t =5s. Active power reference is set at 2 MW and reactive power reference is set at zero. During the fault, distortion in grid current occurs, and thus distortions are seen in active and reactive power. When the fault is cleared the active and reactive power follow the respective references. It also shows the effect of a single line to ground fault on dc link voltage and voltage and current at the point of common coupling.

Fig-7: Response of the system under line to line fault condition.

Fig-7 shows the response of the system under line to line fault condition. The fault occurred at t = 4s and cleared at t =5s. Active power reference is set at 2 MW and reactive power reference is set at zero. During fault distortion in grid current occurs, and thus distortions are seen in active and reactive power. When fault is cleared the active and reactive power follow the respective references. It also shows the effect of line to line fault on dc link voltage and voltage and current at the point of common coupling.
Fig- 8 shows the response of the system under the double line to a ground fault condition. The fault occurred at t = 4s and cleared at t =5s. Active power reference is set at 2 MW and reactive power reference is set at zero. During fault distortion in grid current occurs and thus distortions are seen in active and reactive power. When fault is cleared the active and reactive power follow the respective references. It also shows the effect of double line to ground fault on dc link voltage and voltage and current at the point of common coupling.

Fig- 9 shows the response of the system under three phase fault condition. The fault occurred at t = 4s and cleared at t =5s. Active power reference is set at 2 MW and reactive power reference is set at zero. During the three phase fault, distortion in grid current occurs and thus distortions are seen in active and reactive power. When fault is cleared the active and reactive power follow the respective references. It also shows the effect of three phase fault on dc link voltage and voltage and current at the point of common coupling.

3. CONCLUSION

In this paper, the performance analysis of the Grid Side Converter Control system using FOC algorithm has been examined. Steady-state and dynamic response of the system has been evaluated. The results under various operating conditions show that the system provides a good response. During unbalance of the grid voltage and under different fault conditions the distortion in output current increases significantly. This system provides subsequent accuracy under steady-state and dynamic conditions.

REFERENCES


turbine with permanent magnet synchronous generator. In Innovative Smart Grid Technologies-Asia (ISGT Asia), 2012 IEEE (pp. 1-5). IEEE.


