

Multi-Crop Harvesting Machine

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Abstract - India's economy finds its roots in agriculture. More than 50% of workforce in India is dependent on agriculture. India being the largest producer of many crops like rice, pulses, spices and spice products it export these crops too. Now, as agriculture is this much important to India, farmers of India don't get enough wages out of it and find it difficult to produce required quality and quantity of crops. This is due to high labor cost and highly expensive cultivating machines and as time is moving population of India increases so do the food requirements so taking into consideration all of the above mentioned problems this machine aims to be affordable and efficient. This machine is economical and helps farmer to achieve higher productivity.

Key Words: Bevel Gears, Pulley and Belt drive, chassis

1. INTRODUCTION

Time never stops and it seems growth of India's population too so we need to increase the production of food but there are many barriers come across farmers during food production, which are needed to resolved. There are many machines which can increase the productivity and saves time but those are too costly farmers can't afford them, some of them can, but most part of Indian farmers belongs to middle class and they can't afford it. We require a machine which is efficient as well as economical. This machine aims to be the economical and efficient. Farmers can afford this machine and use it for small scale production, we are aiming for small scale production because most of the farmers who faces problems of labor deficiency and labor costs are producing the crops at small scale.

2. LITERATURE REVIEW

There are two types of harvesting, one of them is manual harvesting and other one is mechanized types of harvesting. The time required in manual harvesting is more than harvesting using machines, it takes approximately 15 to 16 labours to harvest one acre of land in 3 days. The labours being paid 500 to 550 Rupees. Per ton of harvest so total cost of harvesting of one acre of land comes around 30,000 to 35,000 Rupees. In mechanization now by using large scale harvesting machine takes 6 to 7 hours for harvesting of 60 to 70 tons while labour cost is around 4,000

Rupees. Hence total cost occurs is approximately 20,000 to 25,000 Rupees.

- Dr. Sharad S. Chaudhari - His aim is fabricate a small machine to harvest a sugarcane which takes power from petrol engine and different mechanisms. Using this machine sugarcane cut faster rate compare to manual harvesting.
- Joby Bastian - The mechanical properties of the plant material significantly influence the performance of the different unit operation in combine harvester. While checking the mechanical properties it is found that the Young's modulus of the sugarcane stalks as 86MPa, The specific cutting resistance varies between 1764.56 and 957.48 kN/m², penetration resistance ranging from 29.74 kN/m² to 56.33 kN/m² and the crushing force varied from 0.75 kN to 1.53 kN. This study helped us very much while deciding the forces required to cut the cane in one knocking stroke.
- R. R. Price - A fibre optic yield monitoring system was developed for a sugarcane chopper harvester that utilized a duty cycle type approach with three fibre optic sensors mounted in the elevator floor to estimate sugarcane yield. The average observed prediction error on 0.5 to 1.6 Mg estimates was 7.5%; though, the magnitude of the error decreased as the harvested area (tonnage) increased, with an estimated error of 0.03% for 57.8 Mg loads.

3. METHODOLOGY

The idea of the project is to design a crop harvesting machine which is productive and affordable to farmers. The design is so simple that it's easy to disassemble and reassemble if required. The machine takes a power from petrol engine which is mounted on a strong chassis along with all the other parts, the shaft coming out from the engine is horizontal so bevel gears are used to provide the rotation in vertical direction, those bevel gears are connected to a belt and pulley drive which drives the output shaft. Here, two output shafts are provided which are driven through pulley at the bottom of the both the shafts cutters are provided which rotates and harvest the crop, initially the machine is design for sugarcane harvesting as sugarcane requires the high

cutting force so by using that force we can cut other crops too.

4. CALCULATIONS

4.1. Design of Shaft:

Design Torque, N-m $T_d = (60 P \cdot K_t) / 2\pi N$ And we also have $T_d = \pi / 16 \cdot d^3 \cdot \tau_{max}$

Where, d = diameter of shaft

Maximum shear stress,

$\tau_{max} = < 0.18 S_{ut}$ or $< 0.3 S_{yt}$

Selecting material EN8

S_{ut} = ultimate stress = 750 Mpa S_{yt} = yield strength = 465

Mpa From this we get

$\tau_{max} = 0.18 S_{ut} = 139.5$ Mpa

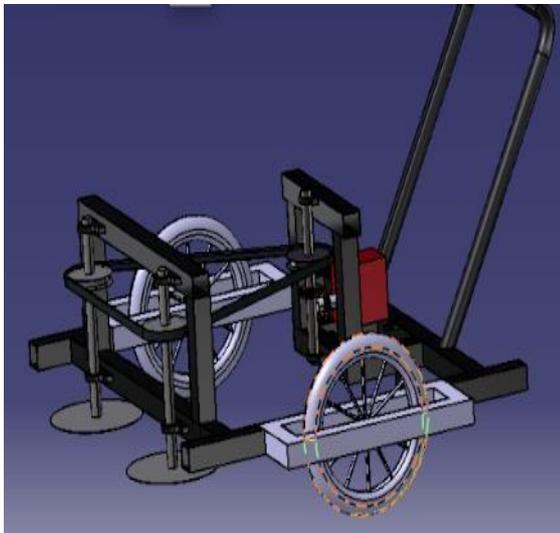


Fig 1- 3D CAD Model

Selecting lower value,

$\tau_{max} = 135$ Mpa

If we used key then we can reduced the stress,

$\tau_{max} = 0.75 \cdot 135 = 101.25$ Mpa

Design Torque, N-m $T_d = (60 P \cdot K_l) / 2\pi N$ And we also have

$T_d = \pi / 16 \cdot d^3 \cdot \tau_{max}$

Where, d = diameter of shaft

$T_d = 2.73632119$ N-m = $\pi / 16 \cdot d^3 \cdot \tau_{max}$

Therefore we get $d = 5.18$ mm. Increase the diameter by 50% to sustaining the various load

$d = d + d \cdot 0.5$ $d = 7.77$ mm

Selecting standard value $d_s = 20$ mm

4.2. Design of bevel gears:

Design power, $P_d = P_r \cdot k_l$

For steady and continuous work

$K_l = 1.25$

Rated power, $P_r = 1$ kW Therefore,

$P_d = 1.25$ kW

$N_P = 3500$ rpm

Assume velocity ratio = 1

Minimum no, of teeth, $T_p = 18$

Therefore, $T_g = T_p$

$T_g = 18$ teeth

$N_g = 3500$ rpm

Pitch angles, γ

For acute angles gears

For pinion,

θ = angle between axes of shafts = 90 degree $\gamma = 45$ degree

$\alpha = 20$ degree

Torque produced,

$M_t = ((60 \cdot 10^6 \cdot 1.25) / 2\pi \cdot 3500) DP = m \cdot Z_p$

$DP = m \cdot 18,$

Now, tooth load, F_t

$F_t = (2 \cdot M_t) / DP,$

$F_t = (2 \cdot 2763.211) / 18 \cdot m, F_t = 307.023 / m$ N

For generated tooth, C_v = velocity factor $C_v = 5.6 / (5.6 + \sqrt{v})$

Effective Load,

$P_{eff} = (C_s \cdot P_t) / C_v = 322.5 / m$

Assume,

$b/L = 1/3$ and $b = 10 \cdot m$

$\tan \gamma = Z_g / Z_p' = 18/18$

Therefore,

$\gamma = 45$

$Z_p' = Z_p / \cos \gamma$ $Z_p' = 18 / \cos (45)$ $Z_p' = 25.455$

Lewis form factor = 0.308

Beam strength, F_b

$F_b = S_b \cdot Y \cdot m \cdot b \cdot (1 - B/L)$ Where,

S_b = bending stress

$S_b = S_{ut} / 3 = 551 / 3$

$S_b = 183.66$ Mpa

$F_b = m \cdot 10 \cdot m \cdot 183.66 \cdot 0.308 [1 - (1/3)],$

$= 377.128 \cdot m^2$

Comparing F_b and F_t ,

$F_{eff} = 322.5 / m \cdot F.O.S = 377.128 \cdot m^2$

$322.5 / m \cdot 2 = 377.128 \cdot m^2$ $m = 1.061$

Standard module, $m = 3$ mm Therefore,

Diameter of gear is $D_g = 54$ mm

Diameter of pinion is $D_p = 54$ mm

Pitch line Velocity,

$V_p = \pi DN / (60 \cdot 1000),$ m/s

$= \pi \cdot 54 \cdot 3500 / (60 \cdot 1000)$ m/s

$V_p = 9.89$ m/s

$F_b = 377.128 \cdot m^2$

$F_b = 3394.152$ N $F_t = 307.023 / m$ N

$F_t = 102.341$ N

$L = 0.5 \sqrt{([D_g]^2 + [D_p]^2)}$ $L = 38.183$ mm

$B = 10 \cdot 3$

$B = 30$ mm

Here,

F_b actual $> F_t$, Hence design is safe and feasible.

Dynamic load

$F_d = F_t + (21 V_p (C_e b + F_t)) / (21 V_p + \sqrt{((C_e b + F_t))})$ Where,

Error = 0.012 mm

$= 102.341 + (21 \cdot 9.89 (11400 \cdot 0.012 \cdot 30 + 102.341)) /$

$(21 \cdot 9.89 + \sqrt{((11400 \cdot 0.012 \cdot 30 + 102.341))})$

$F_d = 3307.72$ N

For finding actual factor of safety.

Beam strength,

$$F_b = m \cdot 10^3 \cdot 233.33 \cdot 0.308 [1 - (1/3)],$$

$$= 377.128 \cdot m^2$$

$$F_b = 3394.152$$

$$F.O.S = F_b / P_e$$

$$= 3394.15 / 3307.72$$

$$F.O.S = 2.66$$

Now for limiting wear strength, F_w

$$F_w = (K_b \cdot D_p \cdot Q) \text{ Where,}$$

$$Q = \text{size factor} = 2T_g / [T_g + T_p \cdot \tan \gamma]$$

$$= 1$$

$$K = 0.75 \cdot [BHN / 100]^2$$

Now,

$$F_w = P_e \cdot F.O.S \text{ Where,}$$

$$P_e = C_s \cdot F_t + F_d$$

$$= 3307.72$$

Therefore,

$$F_w = 3307.72 \cdot 1.026 \text{ Mpa}$$

$$F_w = [0.75 \cdot 30 \cdot 1 \cdot 18 / \cos 45] \cdot [BHN / 100]^2$$

$$\text{From above equations, } BHN = 140.53$$

The material chosen have $BHN > 140.53$, Hence our design is safe and feasible.

4.3. Design of v-belt:

Rated power of Engine, $P_r = 4 \text{ kW}$

Speed of Engine, $N_1 = 5500 \text{ rpm}$ Design Power,

$$P_D = P_r \cdot K_j$$

Loading factor

$$K_j = 1.1 P_D = 4.4 \text{ kW}$$

Now select designation from design power,

Designation is B, Therefore, Diameter of smaller pulley, $d = 100 \text{ mm}$

Diameter of larger pulley

$$D = 1.8 \cdot d$$

$$D = 180 \text{ mm}$$

$$w = 13 \text{ mm, } t = 8 \text{ mm,}$$

Center distance,

$$C = D + 1.5 \cdot d$$

$$C = 180 + 1.5 \cdot 100 = 330 \text{ mm}$$

Length of belt

$$\frac{180 + 100}{2} + 2 \cdot 330 + \frac{(180 - 100)^2}{4 \cdot 330}$$

$$= 1104 \text{ mm}$$

Therefore,

Preferred length from table 13.4 B section, $L = 1100 \text{ mm}$

For Corrected center distance, $L =$

$$1100 \cdot \frac{((100 + 180) / 2 + 2 \cdot C + (180 - 100)^2 / 4 \cdot C)}{C}$$

$$C = 327.64 \text{ mm}$$

Therefore,

Correction factor for Pitch length,

From table 13.34 design data book

V.B.Bhandari for B section, $F_c = 0.85$

Correction factor for arc of length,

From table 13.17,

$$\alpha = 180 - 2 \cdot \sin^{-1} [(D - d) / 2]$$

$$= 165.98 = 166 \text{ degree}$$

From table 13.35, $F_d = 0.97$

Power Rating (P_r) -

From table 13.29, at 2750 rpm, 13mm thick

$$P_r = 2.52 + 0.34 = 2.86 \text{ kW}$$

$$\text{Number of belts, } P \cdot F_a / P_r \cdot F_c \cdot F_d$$

$$= 4 \cdot 1.1 / 2.86 \cdot 0.87 \cdot 0.97$$

$$= 1.82 = 2 \text{ Appx.}$$

4.4. Design of shafts:

A) Shaft carrying bevel gear and pulley

For Force on pulley, F_1

$$\text{Power} = 2 \cdot \pi \cdot N \cdot T / 60$$

$$1 \cdot 10^3 = 2 \cdot \pi \cdot 3500 \cdot T / 60$$

$$T = 2720 \text{ Nmm}$$

Where r = pitch circle radius = 24 mm

F_1 = Total tension force on pulley

$$2720 = F \cdot 0.24$$

Therefore,

$$F_1 = 113.682 \text{ N}$$

For Force on bevel gear, F_2

$$F_t = 102.341 \text{ N } F_r = 26.339 \text{ N } F_a = 26.339 \text{ N}$$

For vertical plane following figure shows bending moment diagram

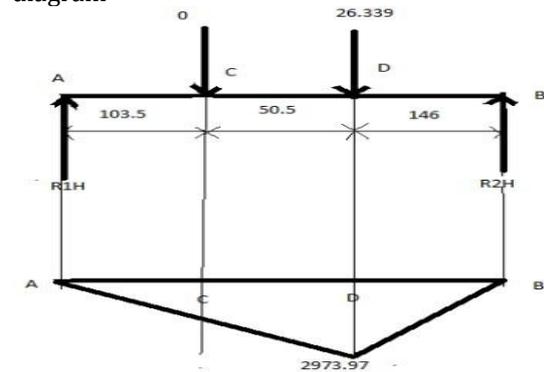


Fig 2 – Bending Moment Diagram

$$R_1 + R_2 = 216.021 \text{ N } R_1 \cdot 300 - 103.34 \cdot 146 = 0$$

$$R_1 = 124.75 \text{ N}$$

$$R_2 = 91.668 \text{ N}$$

Moments,

Moment about c, $M_c =$

$$103.5 \cdot 216.021 = 22358.173 \text{ Nmm}$$

About D, $M_d =$

$$= 216.021 \cdot 154 - 113.68 \cdot 50.5$$

$$= 27526.394 \text{ Nmm}$$

For horizontal plane following diagram shows bending moment diagram,

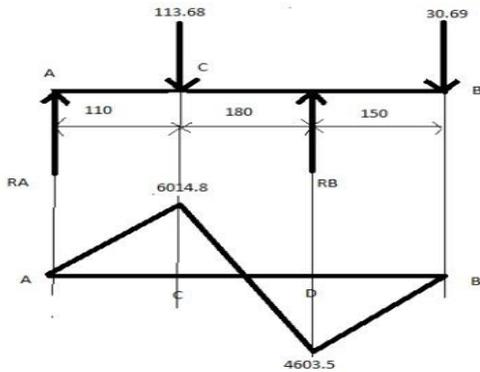


Fig 3 - Bending Moment Diagram

$$R1 + R2 = 26.339 \text{ N} \quad R1 \cdot 300 - 26.339 \cdot 146 = 0$$

$$R1 = 12.818 \text{ N} \quad \text{and} \quad R2 = 13.52 \text{ N}$$

Moment about c, M_c

$$= 0 \text{ N mm}$$

About D, M_d

$$= 12.818 \cdot 154 = 1973.973 \text{ N mm}$$

Therefore,

Resultant bending moment at D,

$$M_d = \sqrt{[(27526.39)^2 + (1973.97)^2]}$$

$$= 27597.077 \text{ N mm}$$

Equivalent Torque by using ASME code,

$$T_{eq} = \sqrt{[(K_b \cdot M_b)^2 + (k_t \cdot T)^2]}$$

Where,

$$K_b = 1.1 \quad \text{and} \quad k_t = 1.5$$

$$T_{eq} = \sqrt{[(1.1 \cdot 27597.07)^2 + (1.5 \cdot 2763.2)^2]}$$

$$T_{eq} = 30638.429 \text{ Nmm}$$

By using Torsional equation,

$$30638.429 = (\pi \cdot D^3 \cdot \tau) / 16$$

$$= (\pi \cdot D^3 \cdot 135) / 16$$

Therefore,

$$D = 10.494 \text{ mm}$$

Selecting standard diameter,

$$D = 20 \text{ mm}$$

B) Shaft carrying pulley and cutter

For Force on pulley, F_1

$$\text{Power} = 2 \cdot \pi \cdot N \cdot T / 60$$

$$1 \cdot 10^3 = 2 \cdot \pi \cdot 3500 \cdot T / 60$$

Therefore,

$$T = 2720 \text{ N mm}$$

Torque,

$$T = F_1 \cdot r$$

F_1 = total tension force on pulley,

$$29997 = F \cdot 24$$

Therefore,

$$F_1 = 113.628 \text{ N}$$

For Force on cutter, F_2

Velocity of cutter

$$V = \pi \cdot D \cdot N / 60,$$

$$= \pi \cdot 0.1778 \cdot 3500 / 60$$

$$= 32.58 \text{ m/s}$$

Therefore,

$$F_2 = 30.69 \text{ N}$$

The fig. below shows free body diagram of shafts,

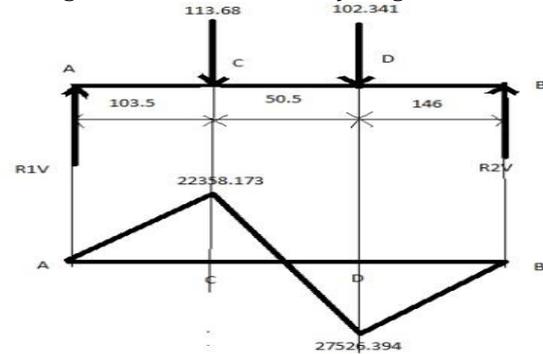


Fig 4 - Bending Moment diagram

For calculating reaction forces, $R_1 + R_2 = 113.682 + 30.69$

$$R_1 \cdot 290 - 113.682 \cdot 180 + 30.69 \cdot 150 = 0$$

Solving above two equations, we get

$$R_1 = 54.687 \text{ N}$$

$$R_2 = 89.685 \text{ N}$$

BM at A = 0,

$$\text{BM at B} = -30.69 \cdot 150 = -4603.5 \text{ N mm}$$

$$\text{BM at C} = -54.687 \cdot 110 = 6014.8 \text{ N mm}$$

Equivalent Torque by using ASME code,

$$T_{eq} = \sqrt{[(K_b \cdot M_b)^2 + (k_t \cdot T)^2]}$$

Where,

K_b = shock and fatigue bending factor k_t = shock and fatigue torsion factor For material EN8

$$K_b = 1.1$$

$$k_t = 1.5$$

$$T_{eq} = \sqrt{[(1.1 \cdot 6014.8)^2 + (1.5 \cdot 2720)^2]} \quad T_{eq} = 7773.1307 \text{ N mm}$$

By using Torsional equation,

$$93798.796 = (\pi \cdot D^3 \cdot \tau) / 16$$

$$= (\pi \cdot D^3 \cdot 135) / 16$$

Hence

$$D = 6.663 \text{ mm}$$

Selecting standard diameter = 20 mm.

4.5. Selection of Bearings:

Diameter of Shaft, $d = 20 \text{ mm}$,

Speed of shaft, $n = 1530 \text{ rpm}$,

Radial component of force, $f_r = 106.75 \text{ N}$

Axial component of force

$$F_a = 0 \text{ N}$$

Bearing Life = $L_{10h} = 12000 \text{ hours}$

Therefore,

$$L_{10} = 60 \cdot n \cdot L_{10h} / 10^6$$

$$= 60 \cdot 3500 \cdot 12000 / 10^6$$

$$= 2520 \text{ million rotations}$$

Dynamic Load Capacity, C Equivalent dynamic loading,
 $P P = Fr$,

Because axial component is zero. $C = P*(L10)^{1/3}$
 $= *(1101)^{1/3}$
 $= 1102.23 \text{ N}$

From table 15.5 From V. B. Bhandari, Following bearings are available for diameter is equal to 20 mm,
 No. 61804 (C = 2700) No. 16404 (C = 7020) No. 6004 (C = 9360)

Therefore, Bearing no. 61804 is selected for above application



Fig 5 - Actual Fabricated Machine

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5. CONCLUSION

This machine is designed with considering all the parameters of actual agricultural field so it is practically applicable for small scale production. The cost of the machine is economical so Indian farmers can afford it. They can use this machine for higher productivity and it also saves time. The problems like labour deficiency and high labour cost can be partially eliminated by using this machine.

6. REFERENCES

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