# COMPARATIVE STUDY OF ANNULAR RAFT FOUNDATION \& SOLID CIRCULAR RAFT FOUNDATION FOR DIFFERENT DIAMETER OF WATER TANK 

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#### Abstract

Storage reservoirs and overhead tank are used to store water, liquid petroleum, petroleum products and similar liquids. The force analysis of the reservoirs or tanks is about the same irrespective of the chemical nature of the product. All tanks are designed as crack free structures to eliminate any leakage. Water is the prime necessity for survival. Liquid storage tanks are used extensively by municipalities and industries for storing water, inflammable liquids and other chemicals. Thus Water tanks are very important for public utility and for industrial structure.


This study attempted the achievement of some measure of the best practical solution, that is, the optimum design of elevated reinforced concrete water tanks for a specified performance in which the major objectives are covers the degree of effectiveness of the geometric shapes for the functional requirement, to assess the possible cost implications of each of the choices and to eventually generate Microsoft Excel Spreadsheet Design Programs as a tool for the rather quick assessment of various tank capacities. The main aim of this dissertation is to done the foundation analysis of circular water tank and cost comparison for different type of foundation required like annular raft and solid circular type raft \& parametric study about time period, hydrodynamic pressure, and seismic pressure respective to $H / D$ ratio.

Key Words: circular water tank, raft foundation soft soil \& medium soil, Seismic pressure, Hydrodynamic pressure, Time period, Staad pro V8i.

## 1. INTRODUCTION

Human civilization has been established long ago. For its development and progress "Civil Engineering" has come into existence, then after there is tremendous continuous progress. In our day-to-day life we see many structures around us, which are the gift of Civil Engineering to human society. There are three basic needs of human namely food, clothes and shelter. The civil engineering satisfy shelter need directly. Further, for the progress of any country good infrastructural facility is required, which is provided by civil engineering. Transportation and Communication facilities plays very important role in improving country's economic growth rate. There are many special civil engineering
structures apart from buildings for example Highways, Bridges, Tunnels, Dams, High-rise Towers, Historical Monuments, Cooling Towers, Nuclear power plants and many more. Elevated Water Tank is also one of them. Reservoir is a common term applied to liquid storage structure and it can be below or above the ground level. Reservoirs below the ground level are normally built to store large quantities of water whereas those of overhead type are built for direct distribution by gravity flow and are usually of smaller capacity. Analysis and design of such tanks are independent of chemical nature of product. In order to avoid leakage and to provide higher strength concrete of grade M25 and above is recommended for liquid retaining structures.

Present study primarily focused on To study the effect of a number of column, batter of column on performance of staging. In addition to the vertical loads is also subjected to horizontal forces. Both these forces produce axial tension or compression in columns as well as moment and shear force on column section. Here attempt is made to find out optimum diameter of staging based on 'No-Tension' in column. Lateral load also affect stability of foundation. Here attempt is made to find out optimum diameter of annular raft footing and solid circular raft footing based on 'NoTension' in foundation and fulfil all stability requirement of foundation including 'No Uplift. comparative study like hydrodynamic pressure, seismic pressure, time period with respect to H/D ratio of different diameter and cost analysis by using annular raft and circular raft foundation for soft soil and medium soil.

## 2. METHODOLOGY

In the present paper consider different diameter of container resting on bottom slab \& circular staging on periphery maintain H/D ration in 0.02 increment, where $\mathrm{H}=$ water height \& $D=$ diameter of tank. Seismic analysis of staging is considered as per IS code 1893 (II) \& concrete design by using staad pro v8i. design of top slab \& bottom slab by using staad pro V8i plate model. Design of annular raft \& circular raft as per code (IS 11089-1984) \& also referred book punamia \& Jain.

Here hydrodynamic effect is considered by dividing water, in the container, into two different masses namely impulsive and convective. When the tank containing liquid with free

International Research Journal of Engineering and Technology (IRJET)
e-ISSN: 2395-0056
Volume: 05 Issue: 04 | Apr-2018
www.irjet.net
p-ISSN: 2395-0072
surface is subjected to horizontal earthquake ground motion, tank wall and liquid are subjected to horizontal acceleration. The liquid in the lower region behaves like a mass that is rigidly connected to the tank wall. This mass is termed as impulsive liquid mass, which, accelerates along with the wall and induces impulsive hydrodynamic pressure on tank wall and on base. The liquid mass in the upper region of tank undergoes sloshing motion. This mass is termed as convective liquid mass and exerts convective hydrodynamic pressure on wall and base. For representing these two masses and in order to include the effect of their hydrodynamic pressure in analysis, spring mass model is adopted for ground-supported tanks and two-mass model for elevated tanks. In spring mass model convective mass ( mc ) is attached to the tank wall by the spring having stiffness Kc, whereas impulsive mass (mi) is rigidly attached to tank wall For elevated tanks two-mass model is considered, which consists of two degrees of freedom system. Spring mass model can also be applied on elevated tanks, but two-mass model idealization is closer to reality. The spring mass model for elevated tank is as shown in fig.2.1.

The response of the two-degree of freedom system can be obtained by elementary structural dynamics. However, for most of elevated tanks it is observed that both the time periods are well separated. Hence, the two-mass idealization can be treated as two uncoupled single degree of freedom system as shown in fig.2.1. The mass (ms) shown in fig.2.1 is the structural mass and shall comprise of mass of tank container and one-third mass of staging as staging will acts like a lateral spring. Mass of container comprises of mass of roof slab, container wall, gallery if any, floor slab, floor beams, ring beam, circular girder, and domes if provided.


Figure - 2.1 Two Mass Idealization Model

Where,
$\mathrm{mi}=$ Impulsive mass
$\mathrm{mc}=$ Convective mass
$\mathrm{ms}=$ Mass of container of elevated tank and one third of staging

Kc = spring stiffness of convective mode
Ks = Lateral stiffness of tank staging
hc = Height at which resultant of convective pressure on wall is located from the bottom of tank wall
hi $=$ Height at which resultant of impulsive hydrodynamic pressure on wall is located from the bottom of tank wall
hi* = Height at which resultant of impulsive hydrodynamic pressure on wall and base is located from the bottom of tank wall
hc* $c^{*}$ Height at which resultant of convective pressure on wall and base is located from the bottom of tank wall

### 2.1 GENERAL CONSIDERATION

Different capacity of circular water tank selected for study purpose. Twelve models are prepare respective soft soil and medium soil where SBC considered $100 \mathrm{KN} / \mathrm{m}^{2} \& 200$ $\mathrm{KN} / \mathrm{m}^{2}$.Primary data considered for design mentioned below.

Table -1: Material and permissible stresses considered for design.

| Grade of concrete | M 30 | MPa |
| :--- | :---: | :--- |
| Grade of reinforcement | 500 | MPa |
| Density of concrete | 25 | $\mathrm{KN} / \mathrm{m}^{3}$ |
| Density of water | 10 | $\mathrm{KN} / \mathrm{m}^{3}$ |
| Modulus of elasticity of <br> concrete (Ec) | 27386 | MPa |
| Modulus of elasticity of steel <br> (Es) | 200000 | MPa |
| Permissible tensile stresses <br> in concrete | 434.783 | $\mathrm{~N} / \mathrm{mm}^{2}$ |
| Permissible stresses in steel | 3.834 | $\mathrm{~N} / \mathrm{mm}^{2}$ |

Table -2: Location and features.

| Seismic Zone | III |
| :--- | :---: |
| z | 0.16 |
| Importance Factor | 1.5 |
| Wind speed $(\mathrm{m} / \mathrm{s})$ | 39 |

International Research Journal of Engineering and Technology (IRJET)
e-ISSN: 2395-0056
Volume: 05 Issue: 04 | Apr-2018

| Terrain Category | 3 |
| :--- | :---: |
| Class | A |
| Type of Soil | Soft \& Medium soil |
| Response Red. Factor | 2.5 |
| K1 | 1.06 |
| K2 | 1 |

### 2.3 ANALYSIS AND CALCULATIONS

The design of overhead circular Water Tank is carried out using the Staad pro V8i. The design is carried out as per relevant analysis procedures combined with Indian Standard Codes of Practices. The water tank top \& bottom slab are designed by Limit stress method. The foundation forces at the level of safe bearing capacity are also evaluated and then manually solid circular raft and annular raft foundation design can be done for diff diameter. The software also gives the shape description of the tank and keeping various parameters, one can change the governing parameter to get the optimum result and safe design with economy.

For analysis purpose considered different type of diameter respective to no of column. In these research maintain H/D ratio. Calculate weight of each component like container in empty \& full condition, top slab, bottom slab, staging etc.

Evolution of seismic analysis and design of column \& bracing used by staad pro V8i. Here 50kl water tank model shown below.


Size of component considered in design and analysis of different diameter of circular water tank like diameter of container, column size, no of bracing and its size, parameter and size of annular raft and circular raft are mentioned below table -3 .

Table -3: Size and component adopted for different diameter of container, staging, bracing, annular raft and circular raft.

| Component | Parameter | Capacity (lit.) |
| :---: | :---: | :---: |
|  |  | 50 KL |
|  | Dia of tank inner (m) | 6 |
|  | Thk of wall (m) | 0.2 |
|  | Height of water (m) | 1.90 |
|  | Free board (m) | 0.4 |
|  | total height (m) | 2.30 |
|  | H/D ratio | 0.32 |
|  | Top Slab Thk (m) | 0.175 |
|  | Dia of top slab (m) | 6.4 |
|  | Bottom Slab Thk (m) | 0.275 |
|  | Dia of bottom slab (m) | 8.8 |
|  | No of staging | 4 |
|  | Staging height (m) | 12 |
|  | Staging dia (m) | 0.45 |
|  | Degree | 90 |
| $\begin{aligned} & \text { U } \\ & \substack{\text { Un } \\ \text { N } \\ \hline} \end{aligned}$ | No of Bracing | 5 |
|  | Size of bracing | $0.3 \times 0.4$ |
|  | Length of bracing | 4.384 |
|  | SBC $100 \mathrm{KN} / \mathrm{m} 2$ |  |
|  | Inner Dia (m) | 4.4 |
|  | outer dia (m) | 8 |
|  | Thk of Raft (m) | $\begin{gathered} \hline 0.400 \text { to } \\ 0.250 \\ \hline \end{gathered}$ |
|  | Inner Dia (m) | 0 |
|  | outer dia (m) | 9.3 |
|  | Thk of Raft (m) | $\begin{gathered} \hline 0.250 \text { to } \\ 0.150 \\ \hline \end{gathered}$ |
|  | SBC $200 \mathrm{KN} / \mathrm{m} 2$ |  |
|  | Inner Dia (m) | 5.2 |
|  | outer dia (m) | 7.2 |
|  | Thk of Raft (m) | $\begin{gathered} 0.300 \text { to } \\ 0.150 \\ \hline \end{gathered}$ |
| $\begin{aligned} & \text { 足 } \\ & \text { S } \\ & \text { 品 } \end{aligned}$ | Inner Dia (m) | 0 |
|  | outer dia (m) | 9.3 |
|  | Thk of Raft (m) | $\begin{gathered} 0.250 \text { to } \\ 0.150 \\ \hline \end{gathered}$ |

Figure - 2.2 Model geometry of staging part and plate model with annular raft in staad pro V8i.

| Component | Parameter | Capacity（lit．） |
| :---: | :---: | :---: |
|  |  | 130 KL |
|  | Dia of tank inner（m） | 8 |
|  | Thk of wall（m） | 0.2 |
|  | Height of water（m） | 2.75 |
|  | Free board（m） | 0.45 |
|  | total height（m） | 3.20 |
|  | H／D ratio | 0.34 |
| $$ | Top Slab Thk（m） | 0.2 |
|  | Dia of top slab（m） | 8.4 |
|  | Bottom Slab Thk（m） | 0.275 |
|  | Dia of bottom slab （m） | 10.8 |
| $\begin{aligned} & \text { U } \\ & \text { U心 } \\ & \text { Su } \\ & \hline \end{aligned}$ | No of staging | 6 |
|  | Staging height（m） | 12 |
|  | Staging dia（m） | 0.5 |
|  | Degree | 60 |
|  | No of Bracing | 5 |
|  | Size of bracing | $0.3 \times 0.4$ |
|  | Length of bracing | 4.1 |
|  | SBC $100 \mathrm{KN} / \mathrm{m} 2$ |  |
|  | Inner Dia（m） | 5.2 |
|  | outer dia（m） | 11.2 |
|  | Thk of Raft（m） | $\begin{gathered} 0.500 \text { to } \\ 0.350 \end{gathered}$ |
|  | Inner Dia（m） | 0 |
|  | outer dia（m） | 12.3 |
|  | Thk of Raft（m） | $\begin{gathered} \hline 0.350 \text { to } \\ 0.250 \end{gathered}$ |
|  | SBC 200 KN／m2 |  |
| 采兒 | Inner Dia（m） | 6.7 |
|  | outer dia（m） | 9.7 |
|  | Thk of Raft（m） | $\begin{gathered} 0.450 \text { to } \\ 0.200 \end{gathered}$ |
|  | Inner Dia（m） | 0 |
|  | outer dia（m） | 12.3 |
|  | Thk of Raft（m） | $\begin{gathered} 0.350 \text { to } \\ 0.250 \end{gathered}$ |


|  | Top Slab Thk（m） | 0.25 |
| :---: | :---: | :---: |
|  | Dia of top slab（m） | 10.4 |
|  | Bottom Slab Thk（m） | 0.3 |
|  | Dia of bottom slab（m） | 12.8 |
| $\begin{aligned} & \text { U } \\ & \text { U心 } \\ & \text { Sús } \end{aligned}$ | No of staging | 8 |
|  | Staging height（m） | 12 |
|  | Staging dia（m） | 0.5 |
|  | Degree | 45 |
|  | No of Bracing | 5 |
|  | Size of bracing | $0.3 \times 0.4$ |
|  | Length of bracing | 3.903 |
|  | SBC $100 \mathrm{KN} / \mathrm{m} 2$ |  |
|  | Inner Dia（m） | 6.2 |
|  | outer dia（m） | 14.2 |
|  | Thk of Raft（m） | $\begin{gathered} 0.500 \text { to } \\ 0.350 \end{gathered}$ |
|  | Inner Dia（m） | 0 |
|  | outer dia（m） | 15.3 |
|  | Thk of Raft（m） | $\begin{gathered} 0.350 \text { to } \\ 0.250 \end{gathered}$ |
|  | SBC 200 KN／m2 |  |
| 彩隻 | Inner Dia（m） | 8.2 |
|  | outer dia（m） | 12.2 |
|  | Thk of Raft（m） | $\begin{gathered} 0.500 \text { to } \\ 0.300 \end{gathered}$ |
|  | Inner Dia（m） | 0 |
|  | outer dia（m） | 15.3 |
|  | Thk of Raft（m） | $\begin{gathered} 0.350 \text { to } \\ 0.250 \end{gathered}$ |


| Component | Parameter | Capacity（lit．） |
| :---: | :---: | :---: |
|  |  | 270 KL |
|  | Dia of tank inner（m） | 10 |
|  | Thk of wall（m） | 0.2 |
|  | Height of water（m） | 3.60 |
|  | Free board（m） | 0.5 |
|  | total height（m） | 4.10 |
|  | H／D ratio | 0.36 |


| Component | Parameter | Capacity (lit.) |
| :---: | :---: | :---: |
|  |  | 485 KL |
|  | Dia of tank inner (m) | 12 |
|  | Thk of wall (m) | 0.2 |
|  | Height of water (m) | 4.55 |
|  | Free board (m) | 0.575 |
|  | total height (m) | 5.13 |
|  | H/D ratio | 0.38 |
|  | Top Slab Thk (m) | 0.3 |
|  | Dia of top slab (m) | 12.4 |
|  | Bottom Slab Thk (m) | 0.4 |
|  | Dia of bottom slab (m) | 14.8 |
| $\begin{aligned} & \text { U } \\ & \text { 눈 } \\ & \text { E } \end{aligned}$ | No of staging | 10 |
|  | Staging height (m) | 12 |
|  | Staging dia (m) | 0.5 |
|  | Degree | 36 |
| $\begin{aligned} & \text { U } \\ & \text { Z } \\ & \text { C } \\ & \text { N } \end{aligned}$ | No of Bracing | 5 |
|  | Size of bracing | $0.3 \times 0.4$ |
|  | Length of bracing | 3.77 |
|  | SBC $100 \mathrm{KN} / \mathrm{m} 2$ |  |
|  | Inner Dia (m) | 6 |
|  | outer dia (m) | 18.4 |
|  | Thk of Raft (m) | $\begin{gathered} \hline 0.750 \text { to } \\ 0.500 \\ \hline \end{gathered}$ |
|  | Inner Dia (m) | 0 |
|  | outer dia (m) | 18.4 |
|  | Thk of Raft (m) | $\begin{gathered} \hline 0.550 \text { to } \\ 0.450 \\ \hline \end{gathered}$ |
|  | SBC $200 \mathrm{KN} / \mathrm{m} 2$ |  |
|  | Inner Dia (m) | 9.7 |
|  | outer dia (m) | 14.7 |
|  | Thk of Raft (m) | 0.6 to 0.4 |
|  | Inner Dia (m) | 0 |
|  | outer dia (m) | 18.4 |
|  | Thk of Raft (m) | $\begin{gathered} 0.550 \text { to } \\ 0.400 \end{gathered}$ |


| Component | Parameter | Capacity (lit.) |
| :---: | :---: | :---: |
|  |  | 830 KL |
|  | Dia of tank inner (m) | 14 |
|  | Thk of wall (m) | 0.25 |
|  | Height of water (m) | 5.60 |
|  | Free board (m) | 0.5 |
|  | total height (m) | 6.10 |
|  | H/D ratio | 0.4 |
|  | Top Slab Thk (m) | 0.35 |


|  | Length of bracing | 3.627 |
| :---: | :---: | :---: |
|  | SBC $100 \mathrm{KN} / \mathrm{m} 2$ |  |
|  | Inner Dia (m) | 4.3 |
|  | outer dia (m) | 28.3 |
|  | Thk of Raft (m) | $\begin{gathered} 1.200 \text { to } \\ 0.750 \end{gathered}$ |
|  | Inner Dia (m) | 0 |
|  | outer dia (m) | 24.5 |
|  | Thk of Raft (m) | $\begin{gathered} \hline 0.950 \text { to } \\ 0.650 \\ \hline \end{gathered}$ |
|  | SBC $200 \mathrm{KN} / \mathrm{m} 2$ |  |
|  | Inner Dia (m) | 11.3 |
|  | outer dia (m) | 21.3 |
|  | Thk of Raft (m) | $\begin{gathered} 1.000 \text { to } \\ 0.650 \\ \hline \end{gathered}$ |
|  | Inner Dia (m) | 0 |
|  | outer dia (m) | 24.5 |
|  | Thk of Raft (m) | $\begin{gathered} 0.900 \text { to } \\ 0.650 \\ \hline \end{gathered}$ |

## 3. RESULTS AND ANALYSIS

After study and analysis of different diameter of water tank respectively annular raft foundation and circular raft foundation perform following result respectively each parameter like time period, base moment, base shear, hydrodynamic pressure, seismic pressure and analysis of cost estimation.

Parametric study and result for time period of impulsive mode and convective mode.

CASE - I: Tank in full condition:-

| Capacity | H/D | Ti | TC |
| :---: | :---: | :---: | :---: |
| 50 KL | 0.32 | 0.878 | 2.823 |
| 130 KL | 0.34 | 0.933 | 3.203 |
| 270 KL | 0.36 | 0.992 | 3.55 |
| 485 KL | 0.38 | 1.143 | 3.851 |
| 830 KL | 0.40 | 1.252 | 4.125 |
| 1275 KL | 0.42 | 1.346 | 4.379 |



CASE - II: Tank in empty condition:-

| Capacity | H/D | Ti | TC |
| :---: | :---: | :---: | :---: |
| 50 KL | 0.32 | 0.803 | NA |
| 130 KL | 0.34 | 0.81 | NA |
| 270 KL | 0.36 | 0.825 | NA |
| 485 KL | 0.38 | 0.924 | NA |
| 830 KL | 0.4 | 0.977 | NA |
| 1275 KL | 0.42 | 1.056 | NA |



Parametric study and result of base shear and base moment for soft soil ( $\mathrm{SBC}=100 \mathrm{KN} / \mathrm{m}^{2}$ ).

|  | Tank in full condition |  | Tank in Empty <br> condition |  |
| :---: | :---: | :---: | :---: | :---: |
| H/D | Base <br> shear | Base <br> moment | Base <br> shear | Base <br> moment |
| 0.32 | 109.236 | 32.768 | 98.366 | 12.714 |
| 0.34 | 189.112 | 112.452 | 161.524 | 13.186 |
| 0.36 | 304.704 | 281.232 | 247.322 | 15.074 |
| 0.38 | 454.604 | 562.974 | 354.72 | 15.143 |
| 0.4 | 643.636 | 1051.214 | 486.145 | 15.417 |
| 0.42 | 981.161 | 1804.381 | 751.964 | 15.604 |

Parametric study and result of base shear and base moment for soft soil ( $\mathrm{SBC}=200 \mathrm{KN} / \mathrm{m}^{2}$ ).

|  | Tank in full condition |  | Tank in Empty <br> condition |  |
| :---: | :---: | :---: | :---: | :---: |
| H/D | Base <br> shear | Base <br> moment | Base <br> shear | Base <br> moment |
| 0.32 | 89.062 | 26.714 | 79.677 | 12.714 |
| 0.34 | 153.955 | 91.53 | 132.156 | 13.186 |
| 0.36 | 248.404 | 229.151 | 201.427 | 13.667 |
| 0.38 | 371.23 | 459.894 | 289.484 | 14.061 |
| 0.4 | 529.242 | 857.143 | 397.216 | 14.719 |
| 0.42 | 807.895 | 1473.578 | 613.444 | 15.241 |

Parametric study and behavior of hydrodynamic pressure and seismic pressure respectively H/D ratio in soft soil (SBC $=100 \mathrm{KN} / \mathrm{m}^{2}$ ).

| Capacity | H/D | Hydrodynamic <br> pressure | Seismic <br> pressure |
| :---: | :---: | :---: | :---: |
| 50 KL | 0.32 | 2.514 | 11.641 |
| 130 KL | 0.34 | 3.302 | 13.407 |
| 270 KL | 0.36 | 4.068 | 15.074 |
| 485 KL | 0.38 | 4.753 | 15.143 |
| 830 KL | 0.4 | 5.595 | 15.417 |
| 1275 KL | 0.42 | 6.491 | 15.604 |




Parametric study and behavior of hydrodynamic pressure and seismic pressure respectively H/D ratio in soft soil (SBC $=200 \mathrm{KN} / \mathrm{m}^{2}$ ).

| Capacity | H/D | Hydrodynamic <br> pressure | Seismic <br> pressure |
| :---: | :---: | :---: | :---: |
| 50 KL | 0.32 | 2.225 | 9.503 |
| 130 KL | 0.34 | 2.966 | 10.916 |
| 270 KL | 0.36 | 3.699 | 12.298 |
| 485 KL | 0.38 | 4.395 | 12.357 |
| 830 KL | 0.4 | 5.235 | 12.495 |
| 1275 KL | 0.42 | 6.12 | 12.828 |




### 3.1 COST ANALYSIS

After safe design and analysis calculate concrete quantity and steel quantity of each part like container, top slab, bottom slab, staging part, annular raft, and circular raft under guide line schedule of rate (SOR) - 2014-15 (section -

International Research Journal of Engineering and Technology (IRJET)
e-ISSN: 2395-0056
Volume: 05 Issue: 04 | Apr-2018
www.irjet.net
p-ISSN: 2395-0072
C),Page 43 to 53.(GUJARAT WATER SUPPLY AND SEWERAGE BOARD).

Cost comparison of annular raft and circular raft for 100 KN/m² (Soft soil).

| Capacity | Annular raft | Circular raft |
| :---: | :---: | :---: |
| 50 KL | ₹ 944,870 | ₹ 987,678 |
| 130 KL | ₹ $1,776,154$ | ₹ $1,798,172$ |
| 270 KL | ₹ $2,659,357$ | ₹ $2,666,777$ |
| 485 KL | ₹ $4,817,682$ | ₹ $4,972,296$ |
| 830 KL | ₹ $7,907,680$ | ₹ $7,698,238$ |
| 1275 KL | ₹ $14,455,964$ | ₹ $12,326,264$ |



Cost comparison of annular raft and circular raft for 200 $\mathrm{KN} / \mathrm{m}^{2}$ (Medium soil).

| Capacity | Annular raft | Circular raft |
| :---: | :---: | :---: |
| 50 KL | ₹ 866,031 | ₹ 981,186 |
| 130 KL | ₹ $1,513,452$ | ₹ $1,775,405$ |
| 270 KL | ₹ $2,292,868$ | ₹ $2,650,888$ |
| 485 KL | ₹ $3,645,373$ | ₹ $4,969,293$ |
| 830 KL | ₹ $5,446,555$ | ₹ $7,426,623$ |
| 1275 KL | ₹ $9,250,402$ | ₹ $11,935,489$ |



## 4. CONCLUSIONS

and study after safe design of circular water tank following conclusion drawn mentioned below respective to annular raft \& solid circular raft in soft soil And medium soil and comparative study of different parameter.

1. As per results and analysis $\mathrm{H} / \mathrm{D}$ ratio vs time period in convective mod and impulsive mode in empty and full condition linearly increase as shown in graph.
2. As per results and analysis H/D ratio vs hydrodynamic pressure and seismic pressure in soft soil ( $100 \mathrm{KN} / \mathrm{m}^{2}$ ) and Medium soil ( $200 \mathrm{KN} / \mathrm{m}^{2}$ ) and full condition linearly increase as shown in graph.
3. When diameter increase and number of column increase the different movement shown in soft and medium soillike in soft soil ( $100 \mathrm{KN} / \mathrm{m}^{2}$ ) up to 12 m diameter of 485 kl capacity of tank resting on 10 circular column annular raft is safe and economical in cost more than solid circular raft and in design more than 12 m diameter solid circular raft is safe and economical in cost shown in graph.
4. In medium soil ( $200 \mathrm{KN} / \mathrm{m}^{2}$ ) diameter increase annular raft is safe and economical in cost more than solid circular raft shown in graph.

## ACKNOWLEDGEMENT

I wish to express my deep sense of gratitude to my guide prof. Farhan Vahora for his valuable guidance and motivation throughout my project work.

I also want to thank our coordinate prof. Abbas jamani for his cooperation and generous help.

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