

# Analysis of damage due to overloading of flexible pavement

Muhammed Shebin<sup>1</sup>, Nikhil Joseph K<sup>2</sup>, Pranav P<sup>3</sup>, Sreejisha K<sup>4</sup>, Prof. Helen Thomas<sup>5</sup>

<sup>1,2,3,4</sup> Under Graduate Students, <sup>5</sup> Professor

<sup>1,2,3,4,5</sup> Mar Athanasius College of Engineering, Kothamangalam, Kerala, India

\*\*\*

**Abstract** – In India the bituminous pavements undergo premature failure much before their design life. There could be many reasons for this premature failure and these include inappropriate selection of materials, lack of dependable traffic and axle load data and limited information related to distresses for analysis. In this paper the nonlinearity in damage of flexible pavement due to overloading and the best tyre configuration for a load without failure were found. The stress-strain analysis of the flexible pavement was carried out using KENLAYER Software. Different tyre configurations were chosen for a particular section for the analysis.

## 1. INTRODUCTION

Overloading is the most important cause of the deterioration of flexible pavements. In developing countries this is very critical, where transportation of heavy vehicles on city roads and highways is increasing. By studies it is found that this problem causes a great damage to road networks and results in high maintenance and repair costs. To overcome this problem one has to develop other branches of transportation such as rail roads, increase the bearing capacity of pavement for the heavier traffic loads, and improve the axle load distribution of overweight vehicles. Ticketing regulations for overweight vehicles can also be introduced so that the users either reduce their loads to the allowable limits or pay compensation fees or fines for the damage.

The stress-strain response of a bituminous pavement depends on the properties of materials used in different layers, traffic on the pavement and the environmental conditions prevalent in the location. In IRC: 37, rutting in subgrade and fatigue cracking initiated at the bottom of the bituminous layers are considered as the two important distresses. The pavements in India experience high temperature around 60°C and above. Using KENLAYER the stresses in the pavement layers due to overloading can be analyzed.

## 2. OBJECTIVES

- To study the nonlinearity in damage to flexible pavement due to overloading
- To study the effect of tyre configuration on damage to flexible pavement

## 3. SOFTWARE

KENLAYER computer program is a most applicable method. Developed by Huang in 1993 and is based on layer theory. KENLAYER together with input program LAYER INP and graphic program LGRAPH is part of a computer package called KENPAVE. Using this software the vertical and tensile stresses can be calculated.

## 4. OVERLOAD-DAMAGE ANALYSIS

A particular pavement section was selected to analyze the overloading-damage relationship. It includes the properties like

|                            |              |
|----------------------------|--------------|
| No. of layers              | : 3          |
| Thickness of sub-base      | : 300mm      |
| Thickness of surface layer | : 100 mm     |
| Modulus of elasticity      |              |
| Subgrade                   | : 77000kPa   |
| Sub-base                   | : 200000kPa  |
| Surface layer              | : 5000000kPa |
| Poisson's ratio            |              |
| Subgrade                   | : 0.4        |
| Sub-base                   | : 0.35       |
| Surface layer              | : 0.35       |
| Contact radius             | : 107.7 mm   |

These data are given to the software. The load was varied as 8t, 16t, 25t, 40t, 50t, 60t, 70t, 80t, 90t, 100t. Even though we are getting stresses at different points of pavement we are choosing the maximum values in each load cases. The output obtained as

| LOAD | TENSILE STRAIN         | VERTICAL STRAIN        |
|------|------------------------|------------------------|
| 8    | 1.972X10 <sup>-4</sup> | 4.082X10 <sup>-4</sup> |
| 16   | 3.945X10 <sup>-4</sup> | 8.165X10 <sup>-4</sup> |
| 25   | 6.166X10 <sup>-4</sup> | 1.276X10 <sup>-3</sup> |
| 40   | 9.866X10 <sup>-4</sup> | 2.042X10 <sup>-3</sup> |
| 50   | 1.233X10 <sup>-3</sup> | 2.553X10 <sup>-3</sup> |
| 60   | 1.48X10 <sup>-3</sup>  | 3.063X10 <sup>-3</sup> |
| 70   | 1.726X10 <sup>-3</sup> | 3.573X10 <sup>-3</sup> |
| 80   | 1.973X10 <sup>-3</sup> | 4.084X10 <sup>-3</sup> |
| 90   | 2.22X10 <sup>-3</sup>  | 4.594X10 <sup>-3</sup> |
| 100  | 2.466X10 <sup>-3</sup> | 5.105X10 <sup>-3</sup> |

IRC: 37-2012 provides two empirical formulae to get the life of pavement.

$$N_F = 2.21 \times 10^{-4} (1/\epsilon_t)^{3.89} (1/E)^{0.854}$$

$$N_R = 4.1656 \times 10^{-8} (1/\epsilon_z)^{4.5337}$$

Where,

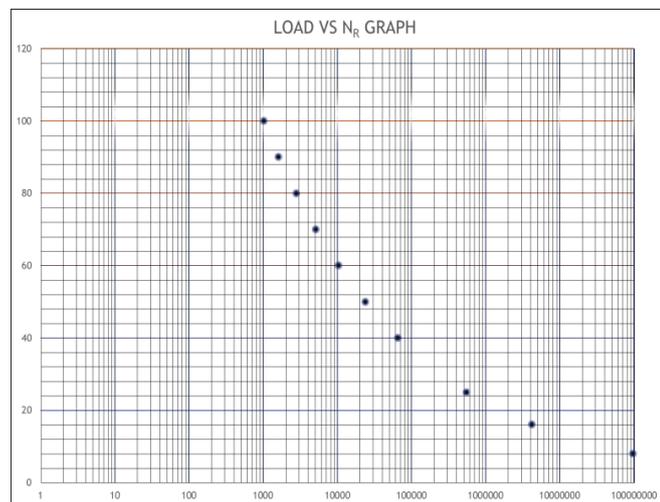
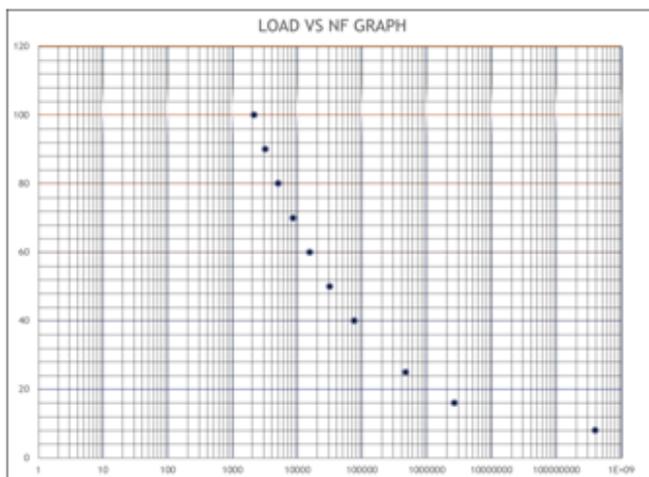
$N_F$  = Cumulative standard axle load repetition before

Pavement develops 20% fatigue cracking

$\epsilon_t$  = Tensile strain at the bottom of surface course

E = Modulus of elasticity of bituminous surfacing

#### 4.1 RESULTS AND DISCUSSIONS



From the Load VS  $N_F$  graph and Load VS  $N_R$  graph it is evident that non-linearity exists for the damages caused by the loads. The conventional way of collecting toll depends on the class of vehicle. For light weight vehicles the chances for overloading is very little when compared to the heavy vehicles like trucks. Since the damages caused by the overloaded trucks are non-linear. So changes should be brought in the conventional method of toll collection.

#### 5. TYRE CONFIGURATION - DAMAGE ANALYSIS

The same pavement section was adopted for this and different tyre configurations were selected from the available list from the site Truck Science, the necessary details were also taken. The details were inserted into the software and the maximum strains were obtained for each configuration.

| CONFIGURATION                                 | VERTICAL STRAIN        | HORIZONTAL STRAIN       |
|---|------------------------|-------------------------|
| DOUBLE AXLE-SINGLE TYRE                       | $1.16 \times 10^{-4}$  | $-6.529 \times 10^{-5}$ |
| FRONT AXLE-SINGLE TYRE<br>REAR AXLE-DUAL TYRE | $8.948 \times 10^{-5}$ | $-3.931 \times 10^{-5}$ |
| TANDEM AXLE                                   | $4.477 \times 10^{-5}$ | $-1.909 \times 10^{-5}$ |
| TRIDEM  | $2.987 \times 10^{-5}$ | $-1.27 \times 10^{-5}$  |

#### 5.1 RESULTS AND DISCUSSIONS

We analysed 4 tyre configurations and obtained the results showing the least strain for TRIDEM configuration which means the least damage is produced by this configuration itself.

#### ACKNOWLEDGEMENT

I express my sincere gratitude and thanks to Dr. Soosan George T, our Principal and Dr. Binoy Alias M, Head of the Department for providing the facilities and all the encouragement and support.

I express my sincere gratefulness to Asst.Prof.Helen Thomas, for her effective motivation, helpful feedback and great support. I express my sincere gratitude to all the faculties of the Department of Civil Engineering for their help and encouragement.

Finally, I would like to acknowledge the heartfelt efforts, comments, criticisms, cooperation and tremendous support given to me by my dear friends during the preparation of the project and also during the presentation without whose support this work would also have been more difficult to accomplish.

#### REFERENCES

- 1) Al-Qadi, I.L., Elseifi, M. A. and Yoo, P. J. (2004) "Pavement Damage to Different Tires and Vehicle Configuration", Michelin Americas Research and Development Corporation Ichelin Americas Research and Development Corporation 515 Michelin Road PO.

- 2) IRC 37:2012, "Guidelines for design of flexible pavements".
- 3) Yang.H.Huang, "Pavement analysis and design", University of Kentucky, Prentice hall, Eaglewood cliffs, New Jersey, 2004.
- 4) Sadeghi, J.M. and M. Fathali, Deterioration Analysis of Flexible Pavements under Overweight Vehicles, Journal of Transportation Engineering, Vol. 133, No. 11, 2007, pp. 625-633.