Performance Analysis of Window Air Conditioning Test Rig

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Abstract - This project is related to the future phase-out of hydro chloro fluoro carbons (HCFCs) used in air conditioning system. Most commonly used refrigerant is R22. In field of refrigeration everyone trying to find alternative refrigerants for R-22. Because hydro chlorofluorocarbons (HCFCs) including R-22 is promised to be banned as per the Montreal protocol. Several refrigerants like R290, R407C, R410A, R134a are emerged as substitutes to replace R-22, the most widely used Fluoro carbon refrigerant in the world. It is become necessary to replace the R-22 by other refrigerants which are environmental friendly. In this project R-290 (hydrocarbon) is selected as alternative for R-22. Because it has zero Ozone Depletion Potential and almost zero Global Warming Potential. The product is typically at least 97.5% pure with minimal level of critical impurities including moisture and unsaturated hydrocarbons. This make it ideal for use in all type of refrigeration systems.

Key Words: Alternate Refrigerant, R22, R290, COP, Cooling Capacity, Energy Efficiency Ratio.

1.INTRODUCTION

In 1974 CFCs were tentatively identified as destructive to the ozone layer. Due to which regular refrigerant R-22 is banned after 2022 for use in refrigeration systems. Hence we select the R-290 (C3H8) as alternative have the low GWP (Global Warming Potential) and zero ODP (ozone Depletion Potential).

1.1 Window Air Conditioner

A window air conditioner is a system that cools space to a temperature lower than the surroundings. To accomplish this, heat must be removed from the enclosed space and dissipated into the surroundings. However, heat tends to flow from an area of high temperature to that of a lower temperature. During the cycle, a substance called the refrigerant circulates continuously through four stages as shown in Fig1. The first stage is called Evaporation and it is here that the refrigerant cools the enclosed space by absorbing heat. Next, during the Compression stage, the pressure of the refrigerant is increased, which raises the temperature above that of the surroundings. As this hot refrigerant moves through the next stage, Condensation, the natural direction of heat flow allows the release of energy into the surrounding air. Finally, during the Expansion phase, the refrigerant temperature is lowered by refrigeration effect. This cold refrigerant then begins the Evaporation stage again, removing more heat from the enclosed space. Window air conditioner works on the principle of vapour compression refrigeration system. The refrigerant is a heat carrying medium which during the cycle in the refrigeration system absorb heat from a low temperature source and discard the heat so absorbed to a higher temperature sink.

1.2 Effect of CFC's:

Ozone layer in Stratosphere up to 50 km from earth's surface protects us against the harmful effects like skin cancer due to UV rays from sun. Ozone layer absorbs the UV radiations and allows only the beneficial heat rays. CFC gases from different reactions on earth goes to this layer and react with ozone which yields different compounds which is known as Ozone layer Depletion. Reaction of R22 with ozone is as shown below:

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**Fig -1: Schematic diagram of Window Air Conditioner**
Sunlight

\[ \text{CH Cl F}_2 \rightarrow \text{CH F}_2 + \text{Cl} \]

\[ \text{O}_3 + \text{Cl} \rightarrow \text{Cl O} + \text{O}_2 \]

Hence Ozone layer depleted to \( \text{O}_2 \)

Solar heat enters through the layer formed by gases emitted from earth and radiated back to space. But as the layer of gases increases heat does not radiated back to space due to which temperature on earth increases which is known as Global Warming. As the CFC refrigerants have chlorine which reacts taking out 100000 \( \text{O}_3 \) molecules.

1.3 Substitute to CFC’s:

The suitability of a refrigerant for a certain application is determined by its physical, thermodynamic, chemical properties and by various practical factors. There is no one refrigerant which can be used for all types of applications. If one refrigerant has certain good advantages, it will have some disadvantages also for a particular application. Hence, a refrigerant is chosen which has greater advantages and less disadvantages.

Although CFC substitutes are of four types i.e. \( \text{N}_2 \), HCFs & HCFCs, HCs and inert gases but basically hydrocarbons and hydro-fluorocarbons are used as alternative refrigerant to CFC refrigerants. As chlorine atom is absent they have zero ODP and less GWP.

We used R290 as alternative to R22 because
- Both are lower boiling and higher pressure refrigerants.
- They require small displacement compressors.

Hence same compressor can be used.

2. EXPERIMENTAL WORK:

2.1 Test Rig Specification:

A LG company window air conditioner of 1 ton refrigeration capacity was selected to be as a test rig. The unit is having single electricity phase rotary compressor. The condenser and evaporator coils are made of copper with smooth inner tube surface. The interrupted type of fin used in the experiment is very widely accepted method of increasing the heat transfer coefficient and creating more turbulent mixing on the air side of heat exchangers. Both compressor and condenser fins were made of aluminum. The conditioner accommodates a three speed motor to run the condenser and evaporator fans. ‘K’ type thermocouples are used at five different locations to record the temperature at condenser inlet, condenser outlet, evaporator inlet, evaporator outlet and comfort air produced by the window air conditioner at the end of cycle.

2.2 Refrigerant charging:

Following steps were performed while gas charging:

i. Connect the bottle, vacuum pump to the valve.

ii. Open the valve between vacuum pump and system connection tubes located in the valve block without opening the main valve of the charging cylinder for removing the air inside the system.

iii. After performing this step kept the system idle for few minutes to check any pressure drop because of leakage.

When all the above steps performed correctly, then gas from the bottle is charge into system.
3. TEST PROCEDURE:

The performance of test is started with providing electrical supply to Test Rig. Further which the main switch is kept on to have electrical supply to all monitoring devices. System was kept in running condition for at least 10 min to achieve steady state. The steady state achievement can be obtained by observing the readings given by temperature indicator and pressure gauge. Further Voltmeter and ammeter reading are also taken into consideration. This test is carried out at ambient temperature and pressure conditions. Three different readings were taken for R22 and R290 at different times. The test were carried out at the highest compressor speed by using speed regulator. Different readings taken are as follows:

i. DBT, WBT At inlet and outlet conditions, in °C
ii. Pressure gauge readings of evaporator (P1) and condenser (P2), in psi.
iii. Energy Meter reading, in kWh.
iv. Voltmeter reading, in Volt.
v. Ammeter reading, in Ampere.

4. OBSERVATION TABLE:

After performing the test following observations were recorded:

<table>
<thead>
<tr>
<th>Table-1: Observation table for R22</th>
</tr>
</thead>
<tbody>
<tr>
<td>Air inlet temperature (°C)</td>
</tr>
<tr>
<td>32.22</td>
</tr>
<tr>
<td>32.86</td>
</tr>
<tr>
<td>33.14</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Table-2: Observation table for R290</th>
</tr>
</thead>
<tbody>
<tr>
<td>Air inlet temperature (°C)</td>
</tr>
<tr>
<td>30.16</td>
</tr>
<tr>
<td>31.34</td>
</tr>
<tr>
<td>30.68</td>
</tr>
</tbody>
</table>

5. CALCULATIONS:

Calculations for R22 and R290 were made with the help of P-h chart and Psychrometric chart. Sample calculations for first reading are as follow:

5.1 For R22:

Assuming mass flow rate as constant, m = 0.145 kg/sec

1. Inlet air enthalpy, \( h_i \) = 75.5 kJ/kg of air
2. Outlet air enthalpy, \( h_o \) = 69.4 kJ/kg of air
3. Enthalpy difference \( h_d = h_i - h_o \) = 75.5-69.4 = 6.1 kJ/kg of air
4. Cooling capacity (C.C.) = mass flow rate of air x Enthalpy difference
   \( = 0.145 \times 6.1 \)
   \( = 0.8845 \text{ kW} \)
   \( = 0.8845 \times 3412.14 \)
   \( = 3018.0370 \text{ Btu/hr} \)
5. Energy Efficiency Ratio (EER) = (C.C. / Energy Meter reading in Whr)
   \( = 3018.0370 / 300 \)
   \( = 10.0601 \)
6. Coefficient of Performance (COP) = EER / 3.412
   \( = 10.0601 / 3.412 \)
   \( = 2.9485 \)

From Pressure – Enthalpy Diagram, we have

Enthalpy at the start of compression, \( h_1 = 403 \text{ kJ/kg} \)
Enthalpy at the end of compression, \( h_2 = 446.5 \text{ kJ/kg} \)
Enthalpy at the start of expansion, \( h_3 = 262 \text{ kJ/kg} \)
Enthalpy at the end of expansion, \( h_4 = 262 \text{ kJ/kg} \)

7. Capacity of the system = 1.5 TR
   \( = 1.5 \times 3.5 \text{ kW} \)
   \( = 5.25 \text{ kW} \)
8. Mass Flow Rate (m) = Capacity in kW/(h_1-h_4)
   \( = 5.25 / (403-262) \)
   \( = 0.03723 \text{ kg/sec} \)
9. Refrigeration Effect (Re) = m x (h_1 – h_4)
   \( = 0.03723 \times (403-262) \)
   \( = 5.2494 \text{ kW} \)
10. Compressor work (W) = m x (h_2 – h_1)
    \( = 0.03723 \times (446.5-403) \)
    \( = 1.6195 \text{ kW} \)
11. Heat rejected in the Condenser \((Q_h)\)

\[ Q_h = m \times (h_2 - h_3) = 0.019944 \times (446.5 - 262) = 6.8689 \text{ kW} \]

12. Co-efficient of Performance (C.O.P.)

\[ \text{C.O.P.} = \frac{(h_1 - h_4)}{(h_2 - h_1)} = \frac{(570 - 306.66)}{(630 - 570)} = 4.389 \]

5.2 For R290:

Assuming mass flow rate as constant, \(m = 0.150 \text{ kg/sec}\)

- Inlet air enthalpy, \(h_1\) = 73.4 kJ/kg of air
- Outlet air enthalpy, \(h_o\) = 65.8 kJ/kg of air
- Enthalpy difference \(h_d = h_1 - h_o\) = 73.4 - 65.8 = 7.6 kJ/kg of air
- Cooling capacity (C.C.) = mass flow rate of air x Enthalpy difference
  \[ = 0.150 \times 7.6 = 1.14 \text{ kW} \]
  \[ = 1.14 \times 3412.1 = 3889.8396 \text{ Btu/hr} \]

5. Energy Efficiency Ratio (EER) = (C.C. / Energy Meter reading in Whr)
  \[ = \frac{3889.8396}{30} = 129.666 \]

6. Coefficient of Performance (COP) = EER / 3.412
  \[ = 12.9666 / 3.412 = 3.8 \]

From Pressure – Enthalpy Diagram, we have
- Enthalpy at the start of compression, \(h_1 = 570 \text{ kJ/kg}\)
- Enthalpy at the end of compression, \(h_2 = 630 \text{ kJ/kg}\)
- Enthalpy at the start of expansion, \(h_3 = 306.66 \text{ kJ/kg}\)
- Enthalpy at the end of expansion, \(h_4 = 306.66 \text{ kJ/kg}\)

7. Capacity of the system = 1.5 TR
  \[ = 1.5 \times 3.5 \text{ kW} = 5.25 \text{ kW} \]

8. Mass Flow rate, \(m\) = Capacity in kW/(\(h_1 - h_4\))
  \[ = 5.25 / (570 - 306.66) = 0.01994 \text{ kg/sec} \]

9. Refrigeration Effect (Re) = \(m \times (h_1 - h_4)\)
  \[ = 0.019944 \times (570 - 306.66) = 5.2498 \text{ kW} \]

10. Compressor Work (W) = \(m \times (h_2 - h_1)\)
    \[ = 0.0243 \times (630 - 570) = 1.1976 \text{ kW} \]

Table-3: Result Table for R22

<table>
<thead>
<tr>
<th>Mass flow rate(m), kg/s</th>
<th>0.03723</th>
<th>0.03697</th>
<th>0.03658</th>
</tr>
</thead>
<tbody>
<tr>
<td>Refrigeration effect, kW</td>
<td>5.2494</td>
<td>5.2497</td>
<td>5.2493</td>
</tr>
<tr>
<td>Compressor work, kW</td>
<td>1.6195</td>
<td>1.6297</td>
<td>1.5912</td>
</tr>
<tr>
<td>Heat rejected ((Q_h)), kW</td>
<td>6.8689</td>
<td>6.8764</td>
<td>6.8404</td>
</tr>
<tr>
<td>COP\text{theoretical}</td>
<td>3.24</td>
<td>3.2272</td>
<td>3.2988</td>
</tr>
<tr>
<td>Cooling capacity, kW</td>
<td>0.8845</td>
<td>0.8990</td>
<td>0.9280</td>
</tr>
<tr>
<td>Energy efficiency ratio</td>
<td>10.0601</td>
<td>10.2250</td>
<td>10.5548</td>
</tr>
<tr>
<td>COP\text{actual}</td>
<td>2.9485</td>
<td>2.9967</td>
<td>3.093</td>
</tr>
</tbody>
</table>

Table-4: Result Table for R290

<table>
<thead>
<tr>
<th>Mass flow rate(m), kg/s</th>
<th>0.01994</th>
<th>0.02022</th>
<th>0.02082</th>
</tr>
</thead>
<tbody>
<tr>
<td>Refrigeration effect, kW</td>
<td>5.2493</td>
<td>5.2491</td>
<td>5.2491</td>
</tr>
<tr>
<td>Compressor work, kW</td>
<td>1.1976</td>
<td>1.2233</td>
<td>1.2498</td>
</tr>
<tr>
<td>Heat rejected ((Q_h)), kW</td>
<td>6.4538</td>
<td>6.4724</td>
<td>6.4989</td>
</tr>
<tr>
<td>COP\text{theoretical}</td>
<td>4.389</td>
<td>4.2909</td>
<td>4.064</td>
</tr>
<tr>
<td>Cooling capacity, kW</td>
<td>1.14</td>
<td>1.155</td>
<td>1.08</td>
</tr>
<tr>
<td>Energy efficiency ratio</td>
<td>12.9666</td>
<td>13.1367</td>
<td>12.2837</td>
</tr>
<tr>
<td>COP\text{actual}</td>
<td>3.8</td>
<td>3.859</td>
<td>3.60</td>
</tr>
</tbody>
</table>
6. COMPARISON OF R22 AND R290

Chart -1: Mass flow rate comparison

Chart -2: Refrigeration effect comparison

Chart -3: Compressor work comparison

Chart -4: Heat rejected comparison

Chart -5: Cooling capacity comparison

Chart -6: Energy efficiency ratio comparison
7. CONCLUSIONS

1. The Energy consumption of Window AC is 20-25 kWh/d/NPT for R290 and 25-30 kWh for R22 kWh/d/NPT

2. Compressor Power: The compressor power required per ton to drive the system is smaller for R290 when compared with R22 taken on average basis.

3. Compressor Ratio: Compressor ratio is lesser for R290 when compared with R22 taken on average basis.

4. Refrigerant Mass flow Rate: The refrigerant mass flow rate per ton is less for R290 when compared with R22 taken on average basis.

5. COP: The Co-efficient of performance of the system for R290 is higher as compared to R22 taken the average of readings. It is observed that COP of R290 is 1.25 times greater than COP of R22.

6. Cooling Capacity: The Cooling Capacity of the system for R290 is better as compared to R22 taken the average of readings.

7. Energy Efficiency Ratio: The Energy Efficiency Ratio of the system for R290 is higher as compared to R22 taken the average of readings.

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