

# PASSIVE COOLING DESIGN FEATURE FOR ENERGY EFFICIENT IN PERI AUDITORIUM

M. Hari Sathish Kumar<sup>1</sup>, K. Pavithra<sup>2</sup>, D.Prakash<sup>3</sup>, E.Sivasaranya<sup>4</sup>,

<sup>1</sup>Assistant Professor, Department of Civil Engineering, PERI Institute of Technology, Chennai 48.

<sup>2,3,4</sup>Student, Department of Civil Engineering, PERI Institute of Technology, Chennai 48

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**Abstract** - IES – Integrated Environmental Solution Passive design responds to local climate and site conditions in order to maximize the comfort and health of building users mean while minimizing energy use. The key to design a passive building is to take best advantage of the local climate. Passive cooling refers to any technologies or design features adopted to reduce the temperature of buildings without the need of power consumption. Energy reduction was achieved by both the harnessing of natural ventilation and minimizing heat gain in line with applying good shading devices alongside the use of double glazing. Additionally green roofing provide its potential by acting as an effective roof insulation. In this project, passive cooling building in “PERI INSTITUTE OF TECHNOLOGY” is designed. The auditorium is designed to provide good acoustic & cooling for many different types of performance specifically lectures, seminar hall, presentation, conference, dramas, etc., our auditorium is free from reverberation effect. The total area of auditorium is 1860Sq.m. with 3000 seats. The plan was done using AUTO CAD. The structural elements like slab, beams, columns and footing are manually designed using IS 456-2000 code book. IS 2526-1963 for auditorium

**Keywords**- passive cooling, energy reduction, ventilation, minimizing heat, shading device.

## 1. INTRODUCTION

Construction is a process that consist of the building or assembling of infrastructures. Structure design is an art and science of designing with economy, safe serviceable and durable structures. The entire process of structural planning and design does not require only imagination and conceptual thinking, but also the structural engineering knowledge of practical aspects such as relevant design codes, laws. Auditorium provides a pleasant environment to the college specially for conducting conference. An auditorium includes any room intendent for listening to music, including theatres, music halls, class room and meeting halls. The design of various, functional, technical, artistic and economical requirements, an auditorium often has to accommodate an unprecedentedly large audience.

Hearing conditions in an auditorium are considerably affected by purely architectural considerations like shape, dimensions, volume, and layout of boundary surfaces, seating arrangements, audience capacity, surface treatment and materials used for interior decoration. Seeing to the increasing use of auditorium in this present scenario, the study of acoustical concepts in “AUDITORIUM DESIGN” is a necessity. So now a day the acoustical concepts are the main considerations in any assembly buildings. By considering the acoustical concepts and control of reverberation defects, we designed “AN ACOUSTIC AUDITORIUM”.

## 2.Slab Design

### DATA

Span of the slab	=	6m×6m
Wall thickness	=	230mm
Grade of cement	=	M-20
Grade of steel	=	Fe-415 HYSD

### CALCULATION

$L_x$	=	6m
$L_y$	=	6m
$l_x/l_y$	=	6/6
	=	1m<2

Since the ratio to long span to short span is less than 2, we are using two way slab.

### TO FIND EFFECTIVE DEPTH

Depth	=	6000/26
Adopt effective depth(d)	=	240mm
Overall depth (D)	=	240+25
	=	265mm

### TO FIND EFFECTIVE SPAN

Effective span	=	(clear span + effective depth)
	=	6.24m

### LOAD

Self-weight of slab	=	6.625kN/m <sup>2</sup>
Live load	=	4kN/m
Floor finish	=	1kN/m <sup>2</sup>
Service load	=	11.6kN/m <sup>2</sup>
Ultimate load	=	1.5×11.625
	=	17.43kN/m <sup>2</sup>

### ULTIMATE MOMENTS AND SHEAR FORCES

By referring (table no:26 of IS 456:2000) and read out the moment co-efficient

$$\begin{aligned} (l_y/l_x) &= 1\text{m} \\ \alpha_x &= 0.047 \\ \alpha_y &= 0.035 \end{aligned}$$

By interpolation method,

$$\begin{aligned} M_{ux} &= (\alpha_x W_u L_x^2) \\ &= 31.89 \text{ kN.m} \\ M_{uy} &= (\alpha_y W_u L_x^2) \\ &= 23.712 \text{ kN.m} \\ V_{ux} &= 0.5 \times W_u \times L_x \\ &= 54.288 \text{ Kn} \end{aligned}$$

### CHECK FOR DEPTH

$$\begin{aligned} M_{max} &= 0.138 f_{ck} b d^2 \\ D &= 107.49 \text{ mm} < 240 \text{ mm} \end{aligned}$$

Effective depth selected is sufficient to resist the design ultimate moment

### REINFORCEMENT

$$\begin{aligned} M_u &= 0.87 f_y A_{st} d [1 - (A_{st} f_y / b d f_{ck})] \\ A_{st} &= 380 \text{ mm}^2 \end{aligned}$$

Adopt 10mm diameter bars

$$\begin{aligned} \text{Spacing} &= (\pi/4) \times 10^2 / 380 \\ &= 206 \sim 250 \text{ mm} \\ \text{No.of.bars} &= 380 / (\pi/4) \times 10^2 \\ &= 4.85 \sim 6 \text{ nos} \end{aligned}$$

Check for shear stress

$$\begin{aligned} \tau_v &= v_u / b d \\ &= 0.226 \text{ N/mm}^2 \\ P_t &= 100 A_{st} / b d \\ &= 0.158 \end{aligned}$$

Table 19 of IS456 – 2000 value is given as

$$\begin{aligned} K.\tau_c &= (1.125 \times 0.32) \\ &= 0.36 \text{ N/mm}^2 \end{aligned}$$

$$K.\tau_c > \tau_v.$$

Hence the shear stress are within safe permissible limit

### 3.Beam Design

#### DATA

$$\begin{aligned} \text{Span} &= 6000 \text{ mm} \\ \text{Width of support} &= 230 \text{ mm} \\ \text{Loads} &= 11.625 \text{ kN/m} \end{aligned}$$

M-20 grade of concrete

Fe-415 grade of steel

### DIMENSION OF BEAM

Provide 230mm width

$$\begin{aligned} \text{Span} &= 6\text{m} \\ d &= 550\text{mm} \\ D &= 600\text{mm} \\ B &= 300\text{mm} \end{aligned}$$

### LOAD CALCULATION

$$\begin{aligned} \text{Self-weight of beam } g &= 22.5 \text{ kN/m} \\ \text{Slab self weight} &= 59.6 \text{ kN} \\ \text{Parapet wall} &= 1.14 \text{ kN/m} \\ \text{Total load} &= 127 \text{ kN/m} \\ \text{Design ultimate load } W_u &= 190.5 \text{ kN/m} \end{aligned}$$

### ULTIMATE MOMENT AND SHEAR FORCE

$$\begin{aligned} M_u &= W_u L^2 / 8 \\ &= 111.04 \text{ kN.m} \\ V_u &= 0.5 W_u L \\ &= 74.01 \text{ kN} \\ M_{u \text{ lim}} &= 0.138 f_{ck} b d^2 \\ &= 167.67 \text{ kN.m} \end{aligned}$$

$M_u < M_{u \text{ lim}}$  section is under reinforced

### AREA OF STEEL REINFORCEMENT

$$\begin{aligned} M_u &= 0.87 f_y A_{st} d [(1 - A_{st} f_y) / (b d f_{ck})] \\ A_{st} &= 775.64 \text{ mm}^2 \end{aligned}$$

Assume 12mm dia bars

$$\begin{aligned} \text{No of bars} &= A_{st} / a_{st} \\ &= 3.85 \sim 4 \text{ nos} \\ \text{Spacing} &= 145.81 \sim 200 \text{ mm} \end{aligned}$$

### CHECK FOR SHEAR STRESS

$$\begin{aligned} V_u &= 74.01 \text{ kN} \\ \tau_v &= V_u / b d \\ &= 0.54 \text{ N/mm}^2 \\ P_t &= 100 A_{st} / b d \\ &= 0.57 \text{ N/mm}^2 \end{aligned}$$

Refer table 19 IS 456:2000

$$\begin{aligned} \tau_c &= 0.42 \text{ N/mm}^2 \\ \tau_c &> \tau_v \end{aligned}$$

Hence beam is safe against shear stress.

### CHECK FOR DEFLECTION CONTROL

$$\begin{aligned} P_t &= 0.57 \\ K_t &= 1.1 \\ K_c &= 1 \\ K_f &= 1 \end{aligned}$$

$$\begin{aligned} (L/d)_{\max} &= (L/d)_{\text{basic}} \times K_f \times K_c \times K_r \\ &= 22 \\ (L/d)_{\text{actual}} &= 6000/550 \\ &= 20 < 22 \\ \text{Hence safe} \end{aligned}$$

#### 4. COLUMN DESIGN

$$\begin{aligned} \text{Column size} &= 230 \times 230 \text{mm} \\ P_u &= 240.725 \text{ kN} \\ M_{ux} &= 15.945 \text{ kNm} \\ M_{uy} &= 11.856 \text{ kNm} \\ f_{ck} &= 20 \text{ N/mm}^2 \\ \text{Assume } d^1/D &= 0.10 \\ b &= 230 \text{mm} \\ D &= 230 \text{mm} \end{aligned}$$

#### EQUIVALENT MOMENT

Reinforcement in the section is designed for the axial compressive load  $P_u$  and the equivalent moment and finally reduced for safety.

$$\begin{aligned} M_u &= 1.15 \sqrt{M_{ux}^2 + M_{uy}^2} \\ &= 22.85 \text{ kNm} \end{aligned}$$

#### NON DIMENSIONAL PARAMETERS

$$(P_u/f_{ck} bD) = 0.22$$

#### REINFORCEMENT

Since the column is under biaxial bending, equivalent reinforcement should be provided on all four sides. Hence using

Chart 44 of sp-16 ( $f_y$  415 N/mm<sup>2</sup>)

$$\begin{aligned} \text{Assume } d^1/D &= 0.10 \\ (P_u/f_{ck} bD) &= 0.22 \\ (M_u/f_{ck} b D^2) &= 0.09 \\ (P/f_{ck}) &= 0.04 \\ &= 0.04 \times f_{ck} \\ &= 0.8\% \\ A_{sc} &= (PbD)/100 \\ &= 423.2 \text{ mm}^2 \\ A_{sc} &= 2\% A_g \\ &= 1058 \text{ mm}^2 \\ \text{No of bars} &= A_{st}/a_{st} \\ &= 3.37 \sim 4 \text{ bars} \end{aligned}$$

Provide 4 bars of 20mm diameter and 4bars of 16mm diameter ( $A_{sc}=190.03$ ) distributed on all faces with 4 bars on each faces

$$(P/f_{ck}) = 0.04$$

Again using chart 44 of SP-16, for

$$(P/f_{ck}) = 0.04$$

$$\begin{aligned} (P_u/f_{ck} bD) &= 0.22 \\ (M_u/f_{ck} b D^2) &= 0.09 \\ M_{ux1} &= 21.90 \text{ kNm} \end{aligned}$$

Because of symmetry

$$M_{ux1} = M_{uy1} = 21.9 \text{ kNm}$$

$$P_{uz} = 466.59 \text{ kN}$$

$$P_u/P_{uz} = 0.515$$

$$P_u/P_{uz} = 0.515$$

From SP16,

$\alpha_n$  is read as 1.5

Check for safety under biaxial bending

$$= [(M_{ux}/M_{ux1})^{\alpha_n} + (M_{uy}/M_{uy1})^{\alpha_n}] \leq 1$$

$$= 0.6 + 0.3 \leq 1$$

$$= 0.9 \leq 1$$

Hence the section is safe against biaxial bending

#### 5. Footing Design

$$\begin{aligned} \text{Total load} &= 240.725 \text{ kN} \\ \text{Bearing capacity} &= 185 \text{ kN/m}^2 \\ \text{Grade of concrete} &= \text{M-20} \\ \text{Grade of steel} &= \text{Fe-415} \\ \text{Column size} &= 230 \times 230 \text{mm} \end{aligned}$$

#### SIZE OF FOOTING

$$\begin{aligned} \text{Load of column} &= 240.7 \text{ kN} \\ \text{Self weight of footing}(10\%) &= 24.07 \text{ kN} \\ \text{Total factored load } W_u &= 264.77 \text{ kN} \\ \text{Footing area} &= 1 \text{ m}^2 \end{aligned}$$

Proportion the footing area in the same proportion as the sides of the columns

Hence,

$$\begin{aligned} (2.3x) \times (2.3x) &= 1 \text{ m} \\ X &= 0.43 \end{aligned}$$

$$\text{Side of footing} = 1 \text{ m}$$

Adopt a square footing of size 1m by 1m

Factored soil pressure at base is completed as:

$$\begin{aligned} P_u &= 240.7 \text{ kN/m}^2 \\ &< 277.5 \text{ kN/m}^2 \end{aligned}$$

Hence the footing area is adequate since the soil pressure developed at the base is less than the factored bearing capacity of soil.

#### FACTORED BENDING MOMENT

$$\begin{aligned} \text{Cantilever projection from the side face of the column} &= 0.5(1-0.23) \\ &= 0.385 \text{ m} \end{aligned}$$

$$\begin{aligned} \text{Bending moment at side face is } (0.5 P_u L^2) &= 17.84 \text{ kNm} \end{aligned}$$

**DEPTH OF FOOTING**

a) Moment considerations :

$$M_u = 0.138 f_{ck} b d^2$$

$$D = 80.39 \sim 100 \text{mm}$$

b) From shear stress considerations we have the critical section for one way shear is located at a distance d from the face of the column

c)

$$V_{ul} = 250(1250 - d) \text{ N}$$

Assuming the shear strength  $\tau_c = 0.36 \text{ N/mm}^2$   
 For M-20 grade % of reinforcements

$$P_t = 0.25$$

Design of reinforcement concrete structures

$$\tau_c = 0.36$$

Hence adopt effective depth d = 520mm  
 Overall depth D = 550mm

**REINFORCEMENT IN FOOTING**

$$M_u = [(0.87 f_y A_{st} d) (1 - A_{st} f_y / b d f_{ck})]$$

$$A_{st} = 558.92 \text{mm}^2$$

Spacing = 360  
 Adopt 16mm diameter bars at 360mm centers  
 Provide 12 mm dia bars,  
 No. of bars = 2.77 ~ 4

**CHECK FOR SHEAR**

The critical section for one way shear is located at a distance d from the face of the columns

Ultimate shear force per metre width in the direction

$$V_u = 175 \text{ kN}$$

$$100 A_{st} / b d = 0.35$$

Refer table 19 of IS 456 - 2000 and read the permissible shear stress

$$= K_s \tau_c$$

$$= 0.42 \text{ N/mm}^2$$

Nominal shear stress

$$\tau_v = v_u / b d$$

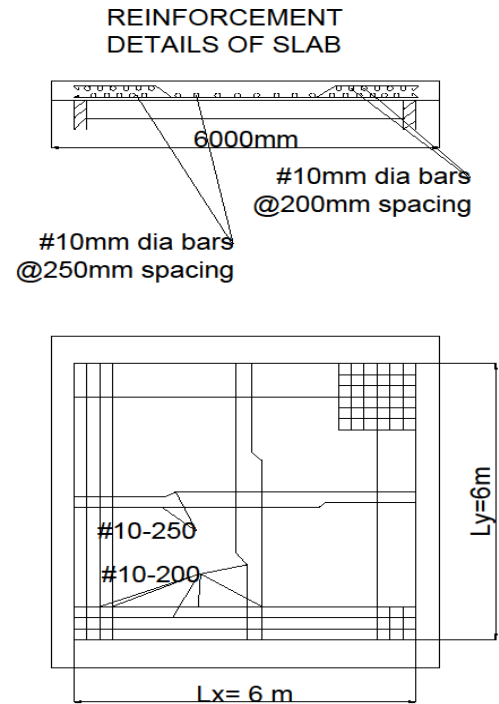
$$= 0.33 \text{ N/mm}^2$$

Since  $\tau_v < K_s \tau_c$

Hence safe.

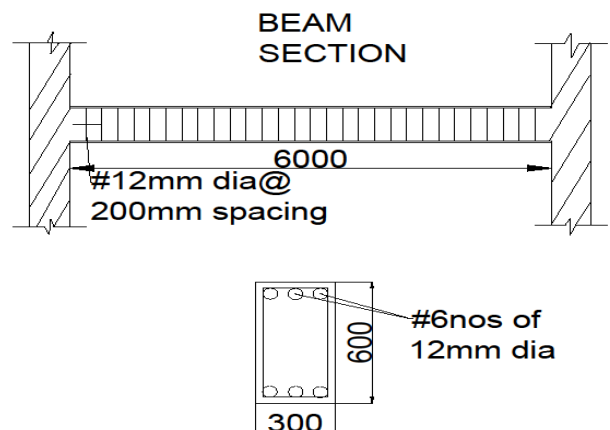
**6. Reinforcement diagrams**

**6.1 Slab**



**Fig. 1: Reinforcement detail of Slab**

**6.2 Beam**



**Fig. 2: Reinforcement detail of Beam**

### 6.3 Plan Of Auditorium & layout

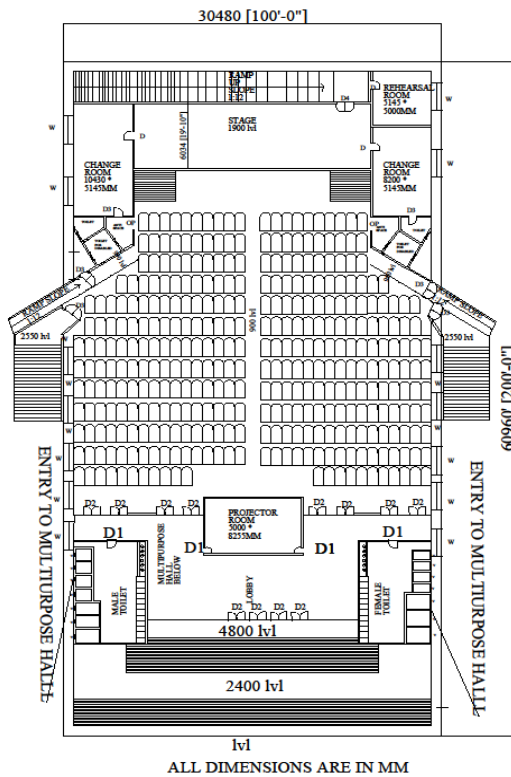


Fig. 3: Plan of an Auditorium

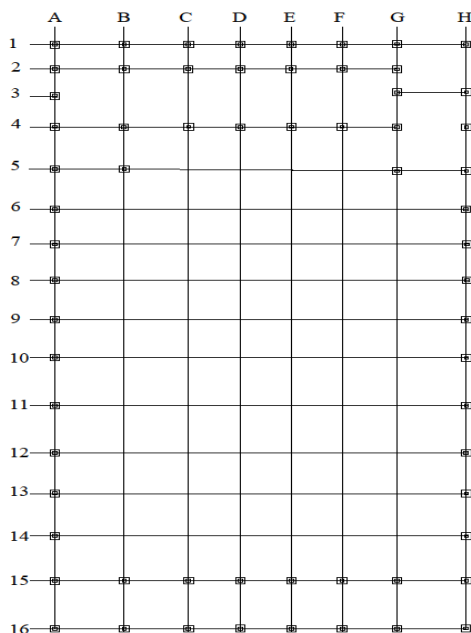


Fig. 4: Column Layout of the Auditorium

### 6.4 Column

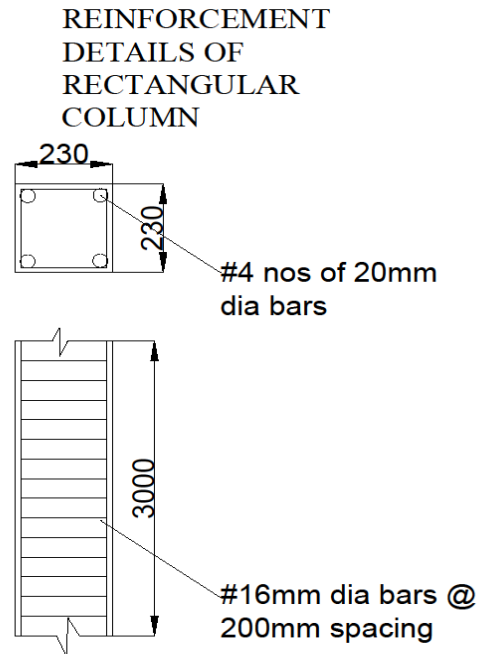


Fig. 5: Reinforcement detail of Column

### 6.5 Footing

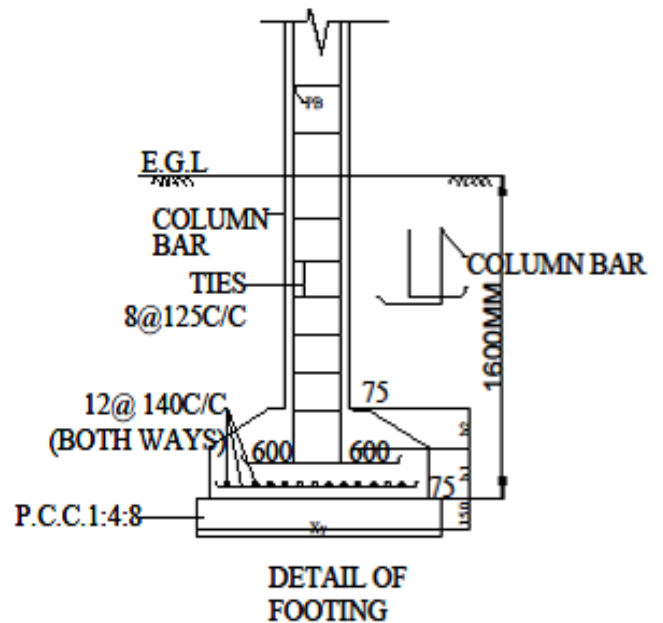


Fig. 6: Reinforcement detail of Footing

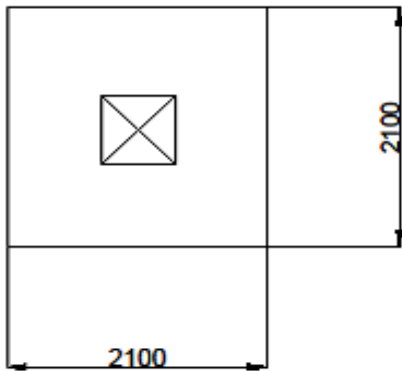


Fig. 7: Layout of Footing

## 7. Result

Table 1: Details of Structural Members

S. NO	ELEMENT	DESIGN PROVIDED
1	SLAB	Depth = 240mm Main reinforcement: 6 nos of 10mm diameter at 200mm spacing
2	BEAM	Depth = 300mm Main reinforcement: 4 nos of 16mm diameter and 12mm diameter at 200mm spacing
3	COLUMN	Diameter:230mm Main reinforcement:4 nos of 20mm dia and 16mm dia at 250 mm spacing
4	FOOTING	Depth:100mm Main reinforcement: 4 nos of 16mm diameter and 16mm diameter at 360mm spacing

## 8. CONCLUSION

Planning and design of auditorium can be considered under an enthusiastic project. The specimen design for structural components like slab, beam, column, and footing are manually done and enclosed with the report. This make the building to give decent finishing without any disturbances and noises. This project implies interest in immense application of various factors involved in the building so this was the main reason for under taking this project. This design reduces the heat

transmission from outside through passive cooling and thereby reducing the usage of the cooling loads and future bills accordingly. Calculations have been done for loads on slabs, beams, columns and after calculating the loads accordingly followed by the footing design.

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