

# A 2D Analytical Investigation of Surface Potential and Electric Field for InSb based Triple Material Gate QWFET

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**Abstract** - In this Paper an analytical model for Two-dimensional Triple Material Gate (TMG) AlInSb/InSb/AlInSb Quantum Well Field Effect Transistor (QWFET) structure have been modeled. In this model, the parabolic approximation method is used to solve **the 2D Poisson's equation by considering the appropriate boundary conditions**. The accurate analytical method for surface potential, electric fields corresponding to the channel position are obtained from this method. The hot carrier effect at the drain side was interpreted from the analytical and simulated output. Also shows that it suppresses electric field at the drain side and enhanced device performance in the sub-nanometer regime. Finally the analytical result is simulated using MATLAB.

**Keywords:** Quantum Well Field Effect Transistor, analytical modeling, 2D Poisson's equation, parabolic approximation, Boundary conditions, surface potential, electric field.

## 1. INTRODUCTION

The invention of electronic machine increases the speed and improves the density of package in miniaturization has been a constant to the nano electronics field. Since it is used in nano electronics field the fabrication of electronic devices should be designed in such a way that the speed of operation should be high. The capabilities of digital **electronics field are strongly associated with Moore's law** [8]. Since it is proven to be accurate it is now used in semiconductor industry to set target for R&D. The quantum well field effect transistor (QWFET) basic structure employs barrier layers of higher band gap materials to avoid device leakage and breakdown. The transistors are mostly fabricated on a semiconductor

substrate. The QWFET [6] takes advantage of quantum tunnelling by increasing the speed of operation of transistor and by avoiding traditional transistor's area of electron transmission.

Gate Engineering technique is used in Triple material gate (TMG) MOSFET. Three different materials having different work functions are merged together in order to produce a single gate of device. In this TMG structure, device ensure low threshold voltage and offers a much lower leakage current, which is because of the work function difference created at the interface of three metals[13-18]. Recently many researchers have modelled HEMT, TFET, MOSFET **characteristics by using 2D Poisson's equation and parabolic approximation methods** but there is not as much in QWFET modelling, so we propose numerical analysis modelling for making accurate results.

Chain [2] proposed a model using GSW equation for HEMT which shows the behavior of electron drift velocity versus electric field, transconductance, channel conductance and gate capacitance. In HEMT structure AlGaAs /GaAs sandwich is used. Arun [4] proposed a 2D analytical model for DMG TFET using parabolic approximation technique and 2D Poisson equation using appropriate boundary conditions. For analyzing the tunneling generation rate and tunneling rate the surface potential and electric field are calculated.

Buckle [3] presents gate leakage currents in InSb/AlInSb QWFET, Gate current is used to obtain barrier heights using Arrhenius style plots. Niaz [1] reports on InAsSb QWFET capacitance voltage (CV) characterization analysis. The 1D coupled Schrodinger Poisson equations were used to analyze electrostatic performance. Based on the characteristics of CV, the physical parameters like oxide thickness, channel thickness were computed.

## 2. MODEL ANALYSIS

The cross sectional view of a Triple Material Gate Quantum Well FET(TMGOWFET) is shown in Fig -1.A DMG Al<sub>0.3</sub>In<sub>0.7</sub>Sb/InSb/Al<sub>0.4</sub>In<sub>0.6</sub>Sb QWFET is used in this

structure. Since our device is TMG, Three gate metals are used. They are M1,M2 and M3.

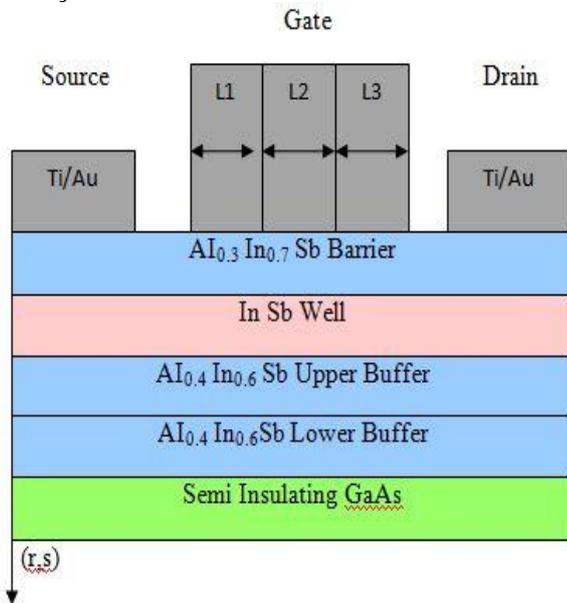


Fig -1: Cross sectional view of a Triple Material Gate Quantum Well FET (TMGQWFET).

The Fig -1 represents the Cross sectional view of a Triple Material Gate Quantum Well FET (TMGQWFET). In this structure, the gate is made of three materials M<sub>1</sub>,M<sub>2</sub> and M<sub>3</sub> of different work functions. The length of those metals are L<sub>1</sub>, L<sub>2</sub> and L<sub>3</sub> where L<sub>1</sub>=10nm,L<sub>2</sub>= 10nm and L<sub>3</sub>=10nm. The total gate length is L=L<sub>1</sub> +L<sub>2</sub>+ L<sub>3</sub>. Ti /Au metallization is used for both source and drain electrodes. QWFET was grown on GaAs substrate. GaAs is exceedingly resistive due to its ample band gap combining with high dielectric constant, this assets makes GaAs an extraordinarily superior electrical substrate than Si. This makes an ideal material for RF circuits. Al<sub>0.3</sub>In<sub>0.7</sub>Sb/InSb/Al<sub>0.4</sub>In<sub>0.6</sub>Sb structure is used as Quantum Well due to its High Electron Mobility Transistor (HEMT), Electron Velocity and Ballistic Length. Al<sub>0.4</sub>In<sub>0.6</sub>Sb layer is used as Upper buffer and Lower buffer over that InSb Well is grown. Al<sub>0.3</sub>In<sub>0.7</sub>Sb is used as a barrier over it. The source and drain regions are uniformly doped. The work function of the metal gate M<sub>1</sub>, M<sub>2</sub> and M<sub>3</sub> is taken as Φ<sub>M1</sub>= 4.8eV, Φ<sub>M2</sub>=4.6eV and Φ<sub>M3</sub>=4.4 eV .

### 2.1 2D-ANALYTICAL MODEL FOR QUANTUM WELL

Let us assume that the impurity density in the Well region is uniform, the 2D potential distribution can be obtained by solving 2D Poisson's equation.

The 2D Poisson's equation is given by,

$$\frac{d^2\phi(r,s)}{dr^2} + \frac{d^2\phi(r,s)}{ds^2} = \frac{qN_A}{\epsilon_w} \quad \text{for } 0 \leq r \leq L, 0 \leq s \leq t_w \quad (1)$$

Where q is the charge of the electron, ε<sub>w</sub> is the dielectric constant of InSb, t<sub>w</sub> is the thickness of InSb Quantum Well, N<sub>A</sub> is the doping concentration, L is the length of gate (i.e.) L=L<sub>1</sub>+L<sub>2</sub> +L<sub>3</sub>. The potential profile in the vertical (S) direction is assumed to be a second order polynomial equation using parabolic function [11].

$$\Phi(r,s) = \Phi_w(r) + W_1(r) s + W_2(r) s^2 + W_3(r) s^3 \quad (2)$$

Where Φ<sub>w</sub>(r) is the Surface potential, W<sub>1</sub>(r), W<sub>2</sub>(r) and W<sub>3</sub>(r) are arbitrary coefficient for the functions of r only. Since it is a TMG structure, the potential is represented for three metals is given by

$$\Phi_1(r,s) = \Phi_{w1}(r) + w_{11}(r)s + w_{12}(r)s^2 + w_{13}(r)s^3 \quad \text{for } 0 \leq r \leq L_1 \text{ at } s = 0 \quad (3)$$

$$\Phi_2(r,s) = \Phi_{w2}(r) + w_{21}(r)s + w_{22}(r)s^2 + w_{23}(r)s^3 \quad \text{for } 0 \leq r \leq L_1 + L_2 \text{ at } s = 0 \quad (4)$$

$$\Phi_3(r,s) = \Phi_{w3}(r) + w_{31}(r)s + w_{32}(r)s^2 + w_{33}(r)s^3 \quad \text{for } 0 \leq r \leq L_1 + L_2 + L_3 \text{ at } s = 0 \quad (5)$$

The boundary condition in the Quantum well is given below:

- (i) Electric flux at the Barrier/Well interface is continuous for TMG QWFET

$$\frac{d\phi_1(r,s)}{ds} = \frac{\epsilon_b}{\epsilon_w} \frac{\Phi_{w1}(r) - \phi_{g1}}{t_b} \quad \text{for Metal 1 at } s = 0 \quad (6)$$

$$\frac{d\phi_2(r,s)}{ds} = \frac{\epsilon_b}{\epsilon_w} \frac{\Phi_{w2}(r) - \phi_{g2}}{t_b} \quad \text{for Metal 2 at } s = 0 \quad (7)$$

$$\frac{d\phi_3(r,s)}{ds} = \frac{\epsilon_b}{\epsilon_w} \frac{\Phi_{w3}(r) - \phi_{g3}}{t_b} \quad \text{for Metal 3 at } s = 0 \quad (8)$$

Where

ε<sub>b</sub> is the dielectric constants of the barrier layer, ε<sub>w</sub> is the dielectric Constants of quantum well layer, t<sub>b</sub> is the thickness of the barrier layer, Φ<sub>w1</sub>(x), Φ<sub>w2</sub>(x) and Φ<sub>w3</sub>(x) are the potential function for M1,M2and M3in barrier/well interface and

Ψ<sub>g1</sub>=V<sub>gs</sub>-V<sub>fb1</sub> , Ψ<sub>g2</sub>=V<sub>gs</sub>-V<sub>fb2</sub> and Ψ<sub>g3</sub>=V<sub>gs</sub>-V<sub>fb3</sub> Where, V<sub>gs</sub> represents the gate source voltage, V<sub>fb1</sub> ,V<sub>fb2</sub> and V<sub>fb3</sub>

represents the flat band voltage under M1,M2 and M3 respectively.

(ii)Electric flux at the Well/ upper Buffer interface is continuous for TMG QWFET

$$\frac{d\phi_1(r,s)}{ds} = \frac{\epsilon_b}{\epsilon_w} \frac{\phi_{w1}(r) - \phi_{g1}}{t_b} \quad \text{for Metal 1 at } s = 0 \quad (9)$$

$$\frac{d\phi_2(r,s)}{ds} = \frac{\epsilon_b}{\epsilon_w} \frac{\phi_{w2}(r) - \phi_{g2}}{t_b} \quad \text{for Metal 1 at } s = 0 \quad (10)$$

$$\frac{d\phi_3(r,s)}{ds} = \frac{\epsilon_b}{\epsilon_w} \frac{\phi_{w3}(r) - \phi_{g3}}{t_b} \quad \text{for Metal 3 at } s = 0 \quad (11)$$

Where

$\epsilon_w$  is the dielectric constants of the Well layer,  $t_{ubu}$  is the thickness of the upper buffer layer,  $\epsilon_{ubu}$  is the dielectric constants of the upper buffer layer,  $\Phi_B(x)$  is the potential function in the well/ upper buffer interface and  $\Psi_{sub} = V_{sub} - V_{fb1}$ ,  $\Psi_{sub} = V_{sub} - V_{fb2}$ , and  $\Psi_{sub} = V_{sub} - V_{fb3}$  where  $V_{sub}$  represents the substrate voltage,  $V_{fb1}$ ,  $V_{fb2}$ ,  $V_{fb3}$  represents the flat band voltage under M1, M2 and M3 respectively.

(iii)Electric flux at the Upper Buffer / Lower Buffer interface is continuous for TMG QWFET

$$\frac{d\phi_1(r,s)}{ds} = \frac{\epsilon_{lbu}}{\epsilon_{ubu}} \frac{\phi_B(r) - \phi_C(r)}{t_{lbu}} \quad \text{for Metal1 at } S = t_{ubu} \quad (12)$$

$$\frac{d\phi_2(r,s)}{ds} = \frac{\epsilon_{lbu}}{\epsilon_{ubu}} \frac{\phi_B(r) - \phi_C(r)}{t_{lbu}} \quad \text{for Metal2 at } S = t_{ubu} \quad (13)$$

$$\frac{d\phi_3(r,s)}{ds} = \frac{\epsilon_{lbu}}{\epsilon_{ubu}} \frac{\phi_B(r) - \phi_C(r)}{t_{lbu}} \quad \text{for Metal3 at } S = t_{ubu} \quad (14)$$

Where  $\epsilon_{lbu}$  is the dielectric constants of the lower buffer layer,  $\epsilon_{ubu}$  is the dielectric constants of the upper buffer layer,  $\Phi_B(r)$ ,  $\phi_C(r)$  is the potential function,  $t_{lbu}$  is the thickness of lower buffer layer.

iv) Potential and Electric flux at three dissimilar metals interface is continuous

$$\Phi_1(L_1,0) = \Phi_2(L_1,0) = \Phi_3(L_2,0) \quad (15)$$

$$\frac{d\phi_1(r,s)}{ds} = \frac{d\phi_2(r,s)}{ds} = \frac{d\phi_3(r,s)}{ds} \quad \text{at } r = L_1 \quad (16)$$

v) Potential at source and drain end is

$$\Phi_1(r,s) = \Phi_{w1}(0) = V_{bi} \quad (17)$$

$$\Phi_1(L,0) = \Phi_{w2}(L) = \Phi_{w3}(L) = V_{bi} + V_{ds} \quad (18)$$

$V_{bi}$  is the built in voltage and  $V_{ds}$  is the drain source voltage

By using the above boundary condition equation (6) to (18) in the parabolic approximation method equation (3),(4)and(5) for calculating the arbitrary coefficient

$w_{11}(r), w_{12}(r), w_{13}(r), w_{21}(r), w_{22}(r), w_{23}(r), w_{31}(r), w_{32}(r), w_{33}(r)$  respectively,

$$w_{11}(r) = c_f \left[ \frac{\phi_{w1}(r) - \phi_{g1}}{\epsilon_w} \right] \quad (19)$$

$$w_{12}(r) = \left[ \frac{\phi_{sub} + \phi_{g1} \left[ \frac{c_f + c_s}{c_b c_s} \right] - \phi_{w1}(r) \left[ \frac{c_f + c_s + 1}{c_b c_s} \right]}{t_{bu}^2 \left[ 1 + \frac{2c_s}{c_b} \right]} \right] \quad (20)$$

$$w_{13}(r) = \frac{[\phi_{g1} \left[ \frac{c_s c_f + c_f}{c_s} \right] - \phi_{sub} \left[ \frac{2\epsilon_{ubu} c_b + c_b^2 w}{c_s c_s} \right] + \phi_B(r) \left[ \frac{2\epsilon_{ubu} c_b + c_b^2 w}{c_s c_s} + 1 \right] - \phi_{w1}(r) \left[ \frac{c_s c_f + c_f + 1}{c_s c_s} \right]}{t_{bu}^2 \left[ 1 + \frac{2c_s}{c_b} \right]} \quad (21)$$

$$w_{21}(r) = c_f \left[ \frac{\phi_{w2}(r) - \phi_{g2}}{\epsilon_w} \right] \quad (22)$$

$$w_{22}(r) = \left[ \frac{\phi_{sub} + \phi_{g2} \left[ \frac{c_f + c_s}{c_b c_s} \right] - \phi_{w2}(r) \left[ \frac{c_f + c_s + 1}{c_b c_s} \right]}{t_{bu}^2 \left[ 1 + \frac{2c_s}{c_b} \right]} \right] \quad (23)$$

$$w_{23}(r) = \frac{[\phi_{g2} \left[ \frac{c_s c_f + c_f}{c_s} \right] - \phi_{sub} \left[ \frac{2\epsilon_{ubu} c_b + c_b^2 w}{c_s c_s} \right] + \phi_B(r) \left[ \frac{2\epsilon_{ubu} c_b + c_b^2 w}{c_s c_s} + 1 \right] - \phi_{w2}(r) \left[ \frac{c_s c_f + c_f + 1}{c_s c_s} \right]}{t_{bu}^2 \left[ 1 + \frac{2c_s}{c_b} \right]} \quad (24)$$

$$w_{31}(r) = c_f \left[ \frac{\phi_{w3}(r) - \phi_{g3}}{\epsilon_w} \right] \quad (25)$$

$$w_{32}(r) = \left[ \frac{\phi_{sub} + \phi_{g3} \left[ \frac{c_f + c_s}{c_b c_s} \right] - \phi_{w3}(r) \left[ \frac{c_f + c_s + 1}{c_b c_s} \right]}{t_{bu}^2 \left[ 1 + \frac{2c_s}{c_b} \right]} \right] \quad (26)$$

$$w_{33}(r) = \frac{[\phi_{g3} \left[ \frac{c_s c_f + c_f}{c_s} \right] - \phi_{sub} \left[ \frac{2\epsilon_{ubu} c_b + c_b^2 w}{c_s c_s} \right] + \phi_B(r) \left[ \frac{2\epsilon_{ubu} c_b + c_b^2 w}{c_s c_s} + 1 \right] - \phi_{w3}(r) \left[ \frac{c_s c_f + c_f + 1}{c_s c_s} \right]}{t_{bu}^2 \left[ 1 + \frac{2c_s}{c_b} \right]} \quad (27)$$

Where

$$c_f = \frac{\epsilon_b}{t_b}, c_b = \frac{\epsilon_{ubu}}{t_{ubu}}, c_a = \frac{\epsilon_{lbu}}{t_{lbu}}, c_s = \frac{\epsilon_w}{t_w}, c_c = \frac{\epsilon_{ubu}}{\epsilon_w} \quad \text{and} \quad c_d = \frac{\epsilon_{ubu}}{t_w}$$

And finally by using the arbitrary coefficient equation (19) to (27) in the parabolic approximation method equation (3) ,(4) and (5) respectively.

The  $\Phi_1(r,s), \Phi_2(r,s)$  and  $\Phi_3(r,s)$  and is obtained, then applying in 2D Poisson's equation (1) to find the surface potential. The surface potential is formed from a second order non homogenous equation with constant coefficients at metals M1, M2 and M3 is given by

$$\Phi_{w_1}(r) = Ae^{\sqrt{v}r} + Be^{-\sqrt{v}r} - \frac{u_1}{v} \quad (28)$$

$$\Phi_{w_2}(r) = Ce^{\sqrt{v}r} + De^{-\sqrt{v}r} - \frac{u_2}{v} \quad (29)$$

$$\Phi_{w_3}(r) = Ee^{\sqrt{v}r} + Fe^{-\sqrt{v}r} - \frac{u_3}{v} \quad (30)$$

Where

$$u_1 = \frac{qN_A}{\epsilon_{si}} - 2\varphi_{g1} \left[ \frac{\frac{\epsilon_f + \epsilon_s}{c_b + c_s}}{t_w^2 \left[ 1 + \frac{2\epsilon_s}{c_{cw}} \right]} \right] - 2\varphi_{sub} \left[ \frac{1}{t_w^2 \left[ 1 + \frac{2\epsilon_s}{c_b} \right]} \right] \quad (31)$$

$$u_2 = \frac{qN_A}{\epsilon_{si}} - 2\varphi_{g2} \left[ \frac{\frac{\epsilon_f + \epsilon_s}{c_b + c_s}}{t_w^2 \left[ 1 + \frac{2\epsilon_s}{c_{cw}} \right]} \right] - 2\varphi_{sub} \left[ \frac{1}{t_w^2 \left[ 1 + \frac{2\epsilon_s}{c_b} \right]} \right] \quad (32)$$

$$u_3 = \frac{qN_A}{\epsilon_{si}} - 2\varphi_{g3} \left[ \frac{\frac{\epsilon_f + \epsilon_s}{c_b + c_s}}{t_w^2 \left[ 1 + \frac{2\epsilon_s}{c_{cw}} \right]} \right] - 2\varphi_{sub} \left[ \frac{1}{t_w^2 \left[ 1 + \frac{2\epsilon_s}{c_b} \right]} \right] \quad (33)$$

$$v = \frac{2 \left[ 1 + \frac{\epsilon_f}{c_b} + \frac{\epsilon_f}{c_s} \right]}{t_w^2 \left[ 1 + \frac{2\epsilon_s}{c_b} \right]} \quad (34)$$

$$A = \frac{[V_{b1} + V_{ds} + X_2] - [e^{\lambda_2(L_1 + L_2)} (V_{b1} - X_1)] - \left[ \frac{X_1 - X_2}{2} \right] (e^{\lambda_1 L_2} + e^{\lambda_2 L_2})}{e^{\lambda_1 L_2} e^{\lambda_2 L_2} - e^{\lambda_2 L_1} + e^{\lambda_2 L_2}} \quad (35)$$

$$B = \frac{[e^{\lambda_1(L_1 + L_2)} (V_{b1} - X_1)] - [V_{b1} + V_{ds} - X_2] + \left[ \frac{X_1 - X_2}{2} \right] (e^{\lambda_1 L_2} + e^{\lambda_2 L_2})}{e^{\lambda_1 L_2} e^{\lambda_2 L_2} - e^{\lambda_2 L_1} + e^{\lambda_2 L_2}} \quad (36)$$

$$C = \frac{[V_{b1} + V_{ds} + X_3] - [e^{\lambda_3(L_2 + L_3)} (V_{b1} - X_2)] - \left[ \frac{X_2 - X_3}{2} \right] (e^{\lambda_2 L_3} + e^{\lambda_3 L_3})}{e^{\lambda_2 L_3} e^{\lambda_3 L_3} - e^{\lambda_3 L_2} + e^{\lambda_3 L_3}} \quad (37)$$

$$D = \frac{[e^{\lambda_2(L_2 + L_3)} (V_{b1} - X_2)] - [V_{b1} + V_{ds} - X_3] + \left[ \frac{X_2 - X_3}{2} \right] (e^{\lambda_2 L_3} + e^{\lambda_3 L_3})}{e^{\lambda_2 L_3} e^{\lambda_3 L_3} - e^{\lambda_3 L_2} + e^{\lambda_3 L_3}} \quad (38)$$

$$E = C \exp(\lambda_2 L_2) + \left( \frac{\lambda_2 - \lambda_3}{3} \right) \quad (39)$$

$$F = D \exp(\lambda_3 L_2) + \left( \frac{\lambda_2 - \lambda_3}{3} \right) \quad (40)$$

Where

$$X_1 = \frac{-u_1}{v}, X_2 = \frac{-u_2}{v} \text{ and } X_3 = \frac{-u_3}{v}$$

$$E_1(r) = \frac{d\Phi_1(r,s)}{dr} = \frac{d\Phi_{w_1}(r)}{dr} = A\sqrt{\mu} e^{\sqrt{\mu}r} - B e^{-\sqrt{\mu}r}$$

$$\text{for } 0 \leq r \leq L_1 \quad (41)$$

$$E_2(r) = \frac{d\Phi_2(r,s)}{dr} = \frac{d\Phi_{w_2}(r)}{dr} = C\sqrt{\mu} e^{\sqrt{\mu}(r-L_1)} - D e^{\sqrt{\mu}(r-L_1)}$$

$$\text{for } L_1 \leq r \leq L_1 + L_2 \quad (42)$$

$$E_3(r) = \frac{d\Phi_3(r,s)}{dr} = \frac{d\Phi_{w_3}(r)}{dr} = C\sqrt{\mu} e^{\sqrt{\mu}(r-L_1+L_2)} - D e^{\sqrt{\mu}(r-L_1+L_2)}$$

$$\text{for } L_1 + L_2 \leq r \leq L_3 \quad (43)$$

### 3. RESULTS AND DISCUSSIONS

The analytical model of InSb TMG QWFET is solved in section 2. It is necessary to verify the workout model by using 2D device simulation. For a voltage 0-0.5 V of  $V_{ds}$ , the gate bias induces an accumulation of electrons in the channel region. This leads to reduce channel resistance. Hence the well width is decreased which in turn increases the electric field across the well junction.

Fig -2 shows the simulated surface potential of TMG QWFET by varying  $V_{gs}$  the gate source voltage consider for this evaluation is 0.2, 0.1 V respectively. The channel length is considered to be 30nm and  $V_{ds}=0.1V$  It depicts that as the gate voltage increases the surface potential also increases there is a step change of 0.4V in potential along the channel at the interface of  $M_1, M_2$  and  $M_3$ .

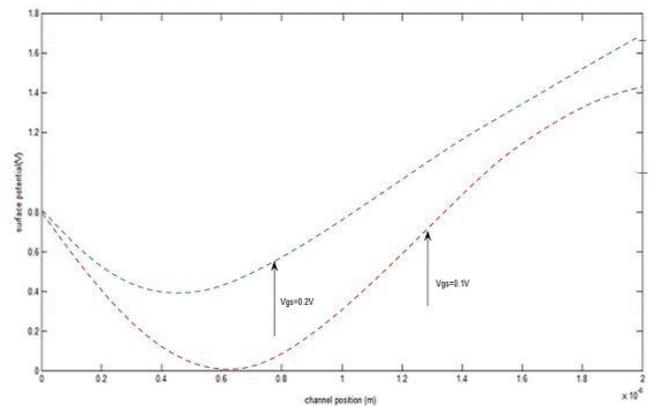


Fig -2: Surface potential of TMG QWFET with various gate source voltage.

Fig -3 shows the simulated output of electric field along the channel length with different  $V_{gs}$  It is evident from the figure that peak of the electric field appears near the other Metals. Thus electric field near the source decrease with the change in work function with different metals Such as  $M_1, M_2, M_3$ .

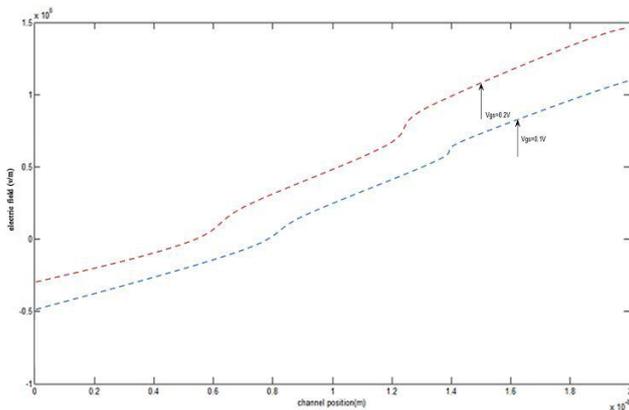


Fig -3: Electric field with various  $V_{gs}$ .

Fig-4 The work function considered for  $M_1, M_2$ , and  $M_3$  respectively. The electric field is gradually throughout the channel  $L$  ( $L_1+L_2+L_3$ ). The electric field at the source is very less whereas the electric field increases at the drain region.

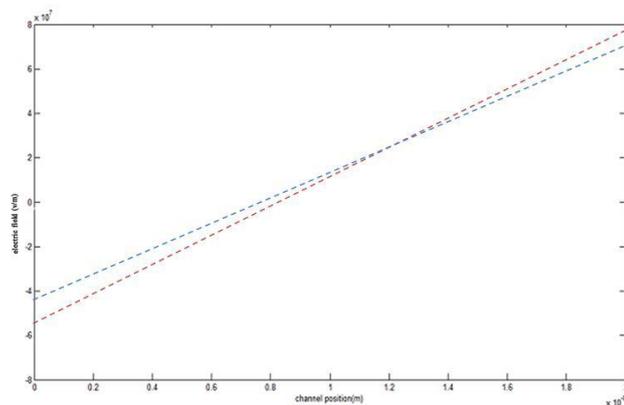


Fig -4: Various work function of  $M_1, M_2$  and  $M_3$

Table – 1: Values used for MAT LAB simulation.

Barrier thickness	50nm
Well thickness	70nm
Buffer thickness	20nm
Doping concentrations	$10^{20} \text{cm}^{-3}$
Channel length ( $L_1+L_2+L_3$ )	$30\text{nm}+30\text{nm}+30\text{nm} = 90\text{nm}$

#### 4. CONCLUSION

An analytical model for InSb based TMG QWFET using 2D Poisson equation and boundary conditions, the surface potential and electric field analysis was formed. Thus we understand that one metal in gate is screened off due to the effect of drained voltage. The electric field at the drain side is reduced by the carriers in the channel which can be

interpreted as the decrease of hot carrier effect at drain side. The proposed analytical method shows an excellent equality while comparison with other design.

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